



Silesian
University
of Technology



RESEARCH
UNIVERSITY
EXCELLENCE INITIATIVE
Ministry of Science
and Higher Education



Materials Engineering
Faculty



Materials Technologies
Department

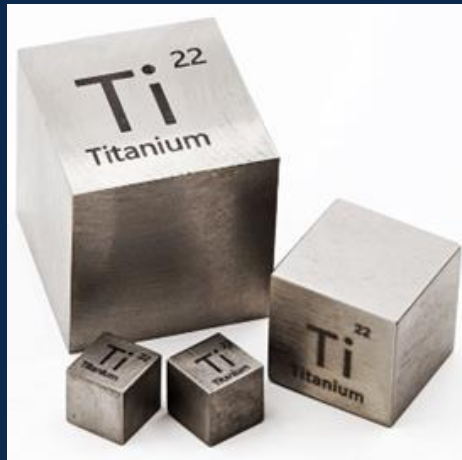
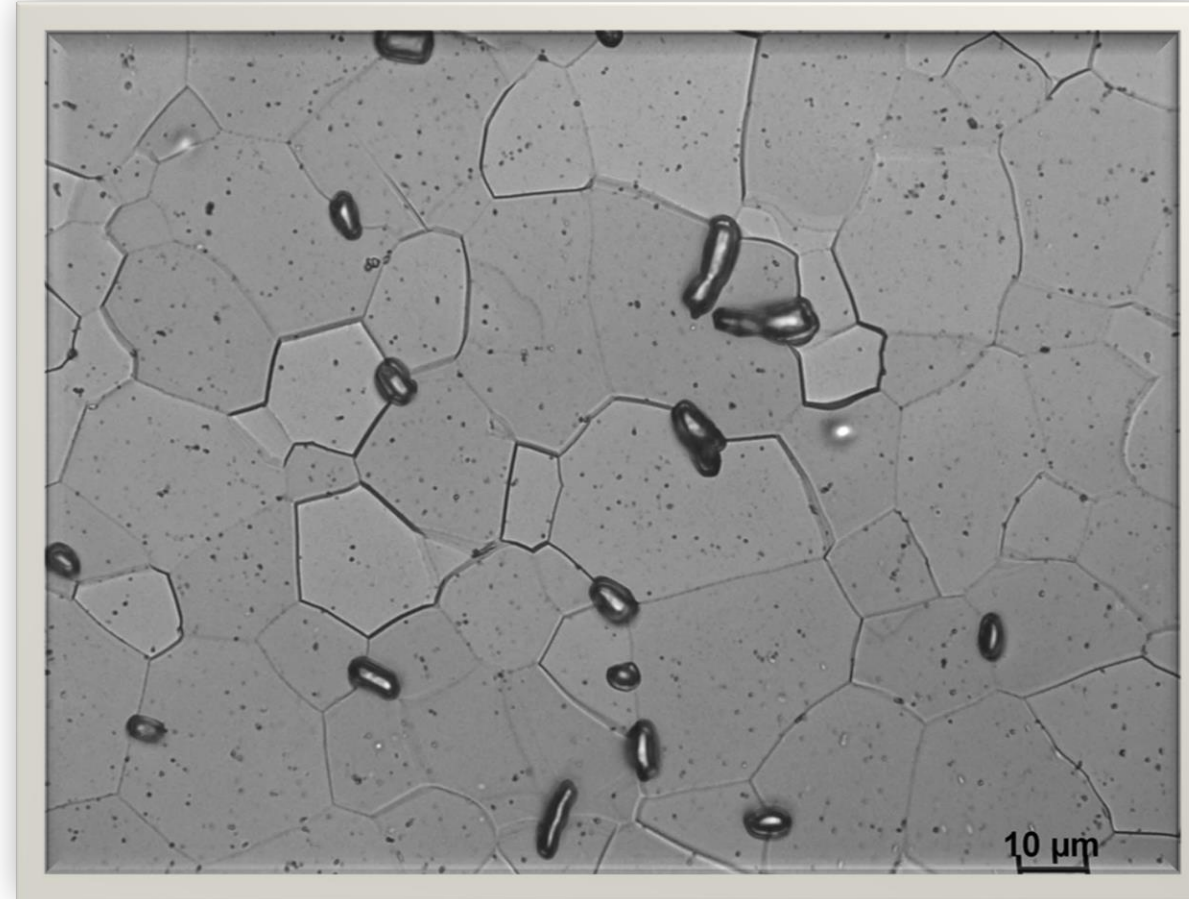
CARBON IN TITANIUM ALLOYS – PROBLEMS OR BENEFITS

Dr hab. inż. Agnieszka Szkliniarz prof. PŚ



Materials Engineering Forum 30.06.2022

Plan of presentation



1. Introduction
2. Classical titanium alloys melted in ceramic crucibles
3. Titanium aluminides melted in graphite crucibles
4. Titanium alloys with carbon
5. Summary



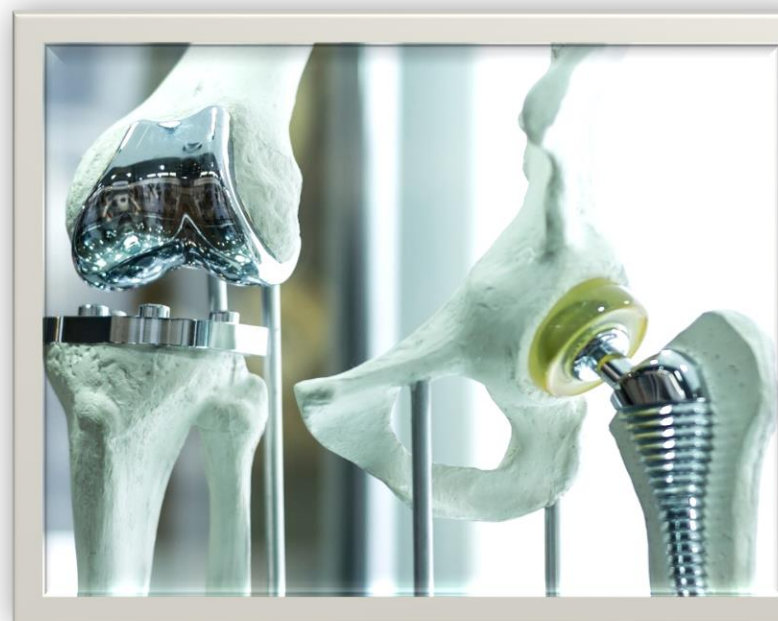
Introduction: Market of titanium

Aerospace

Biomaterials

Military

Automotive



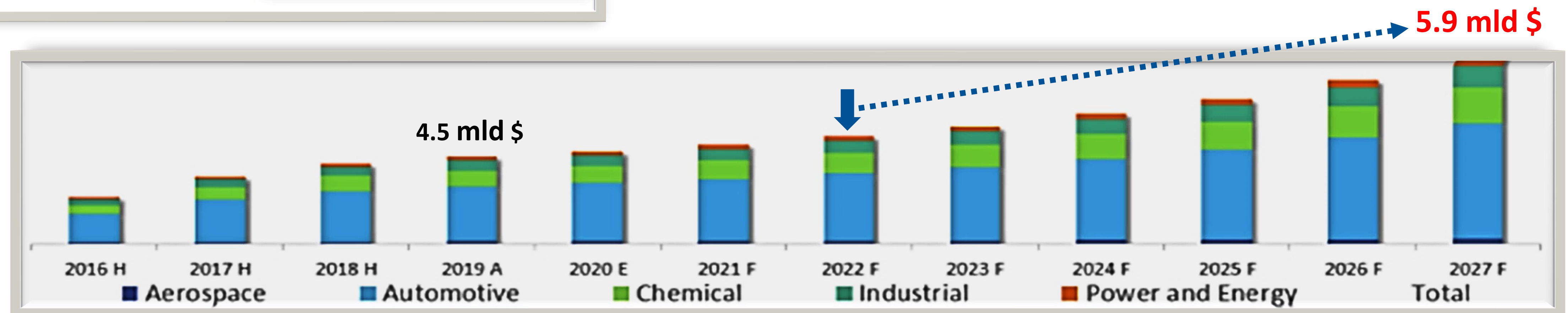
Aerospace Titanium Market by Aircraft Type



Aerospace Titanium Market by Application



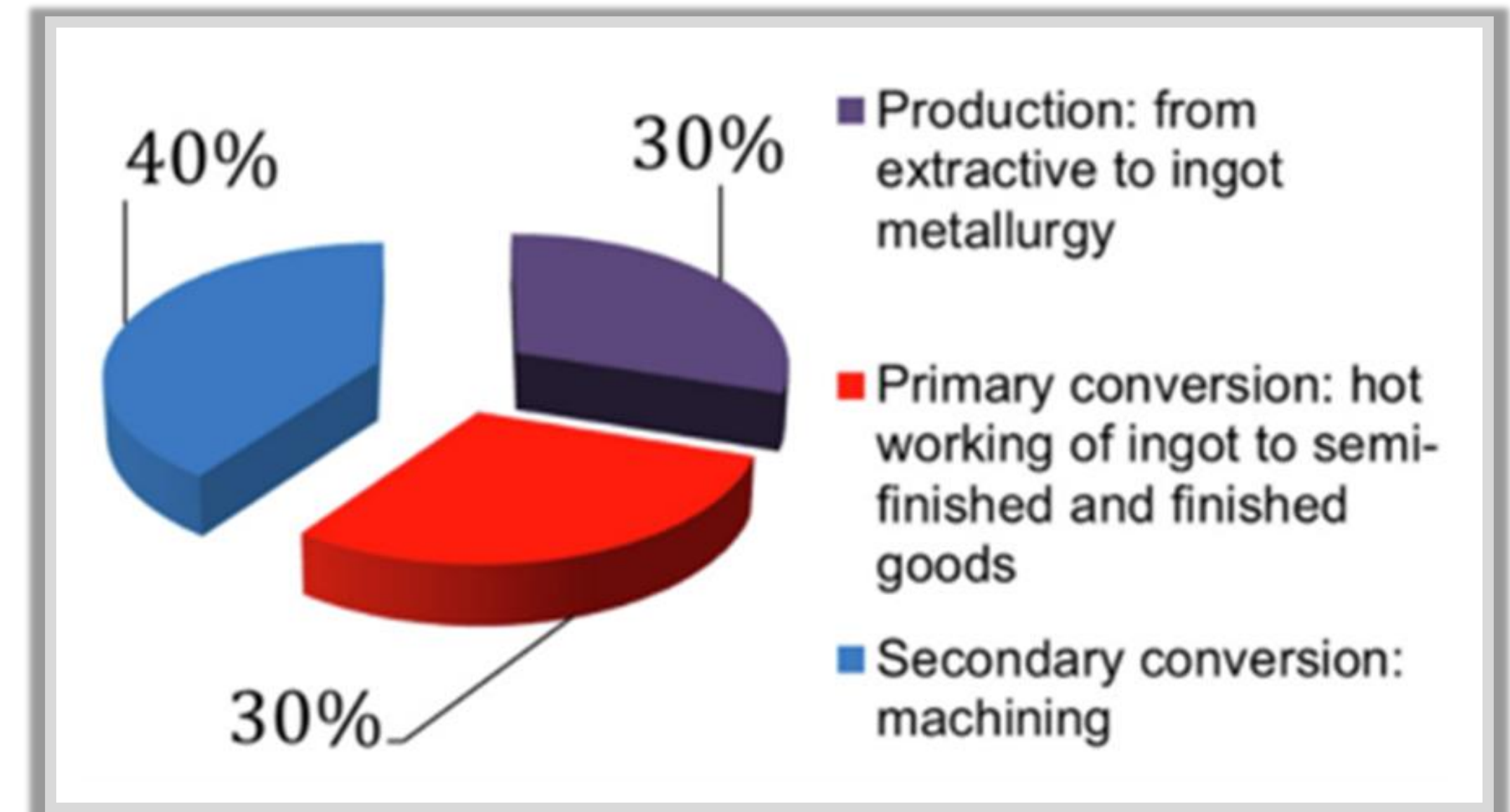
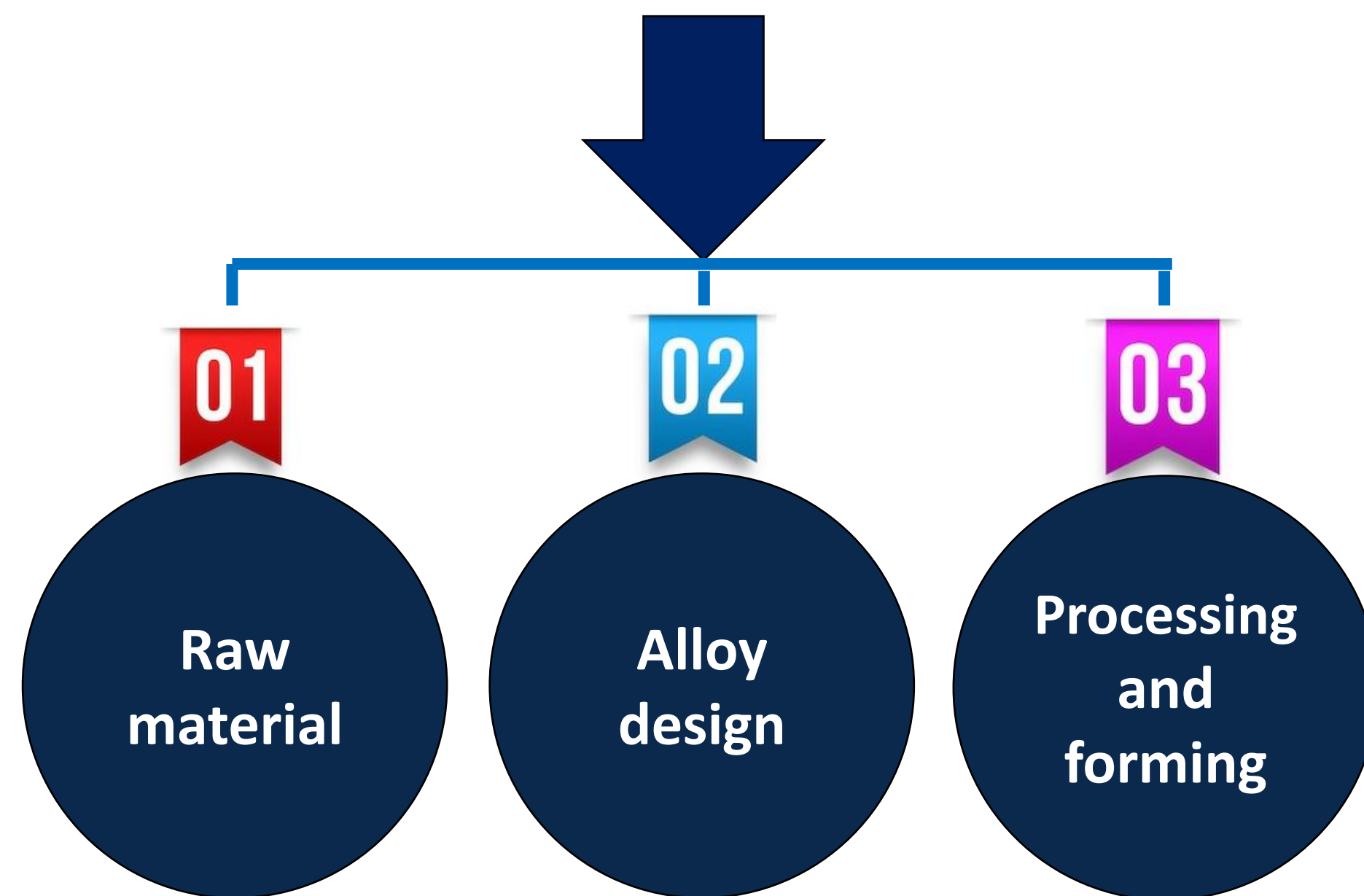
CAGR: Negative <0% ↓ Flat 0%-3% → Growing >3% ↑



Introduction: Low cost titanium alloys

Critical factors contribute to the cost of producing titanium alloys:

- High cost of titanium sponge production
- expensive and rare alloying elements
- **complex and multi-staged hot working**
- **difficult machining**



Processing step to total cost of titanium alloys



Introduction: Low cost titanium alloys – possibility of cost reduction

Development of cheapest and easy method of pure titanium production

- titanium tetrachloride electrolysis method,
- continuous liquid reduction method,
- flow continuous gas phase smelting method,
- direct electrolysis reduction of titanium dioxide,
- use of revert materials,
- compact processes for high efficiency fabrication based on electron beam (EB) cold hearth smelting.

Substitution of expensive alloying elements

- use cheap alloying elements to instead of expensive alloying elements without reducing the performance of the alloy
- design low cost titanium alloy which is not sensitive to impurity elements and made with revert material

5-20%

Optimization of hot working and machining processes

- near net forming technology: low-cost powder metallurgy technology. superplastic forming/ diffusion bonding. casting. laser melting deposition additive manufacturing
- Conception of „fast technology”

50%

IMPORTANT!

Establish the classification standards for low-cost titanium alloys used in different industries



**Silesian University
of Technology**

Based on M. Bodurin et al.: Development of low-cost titanium alloys: A chronicle of challenges and opportunities. Materials Today: Proceedings. 2021



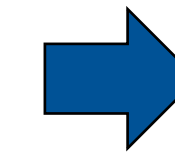
Introduction: Low cost titanium alloys – example / trend in alloy design strategy

Ti 6Al-4V

Cost reduction approach

reduce Al
replace Al with O and N
replace V with Fe
replace V with Cr and Mn

Interstitial elements
Alpha phase stabilizer



Experimental titanium alloys

Ti-1.5Fe-0.49O-0.05N

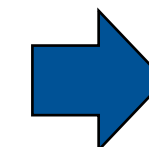
Ti-3.5Al-1Fe. Ti-5.5Al-1Fe.

Ti-3Al-2.1Cr-1.3Fe

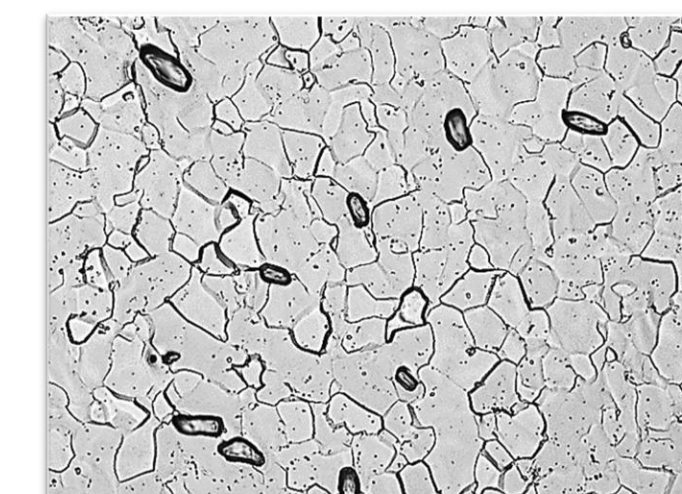
Ti-4.5Al-6.9Cr-2.3Mn

Ti-4.5Al-1V-3Fe. Ti-6Al-1V-3Fe

Ti-xC



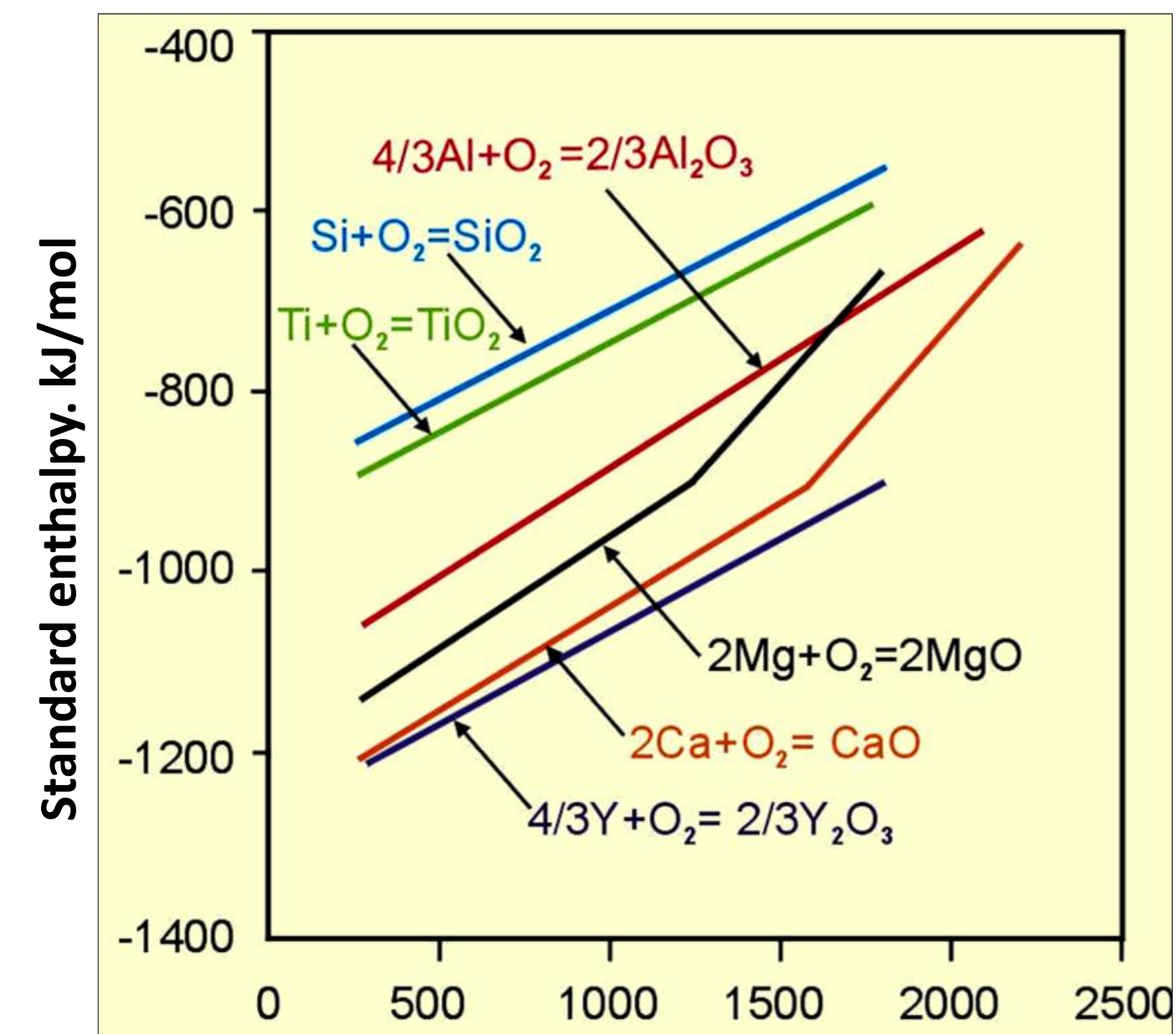
+



2. TITANIUM ALLOYS MELTED IN CERAMIC CRUCIBLES



Materials Engineering Forum 30.06.2022



C(grafit) → SiC → SiO₂ → MgO → Al₂O₃ → ZrO₂ → CaO → Y₂O₃ → Cu



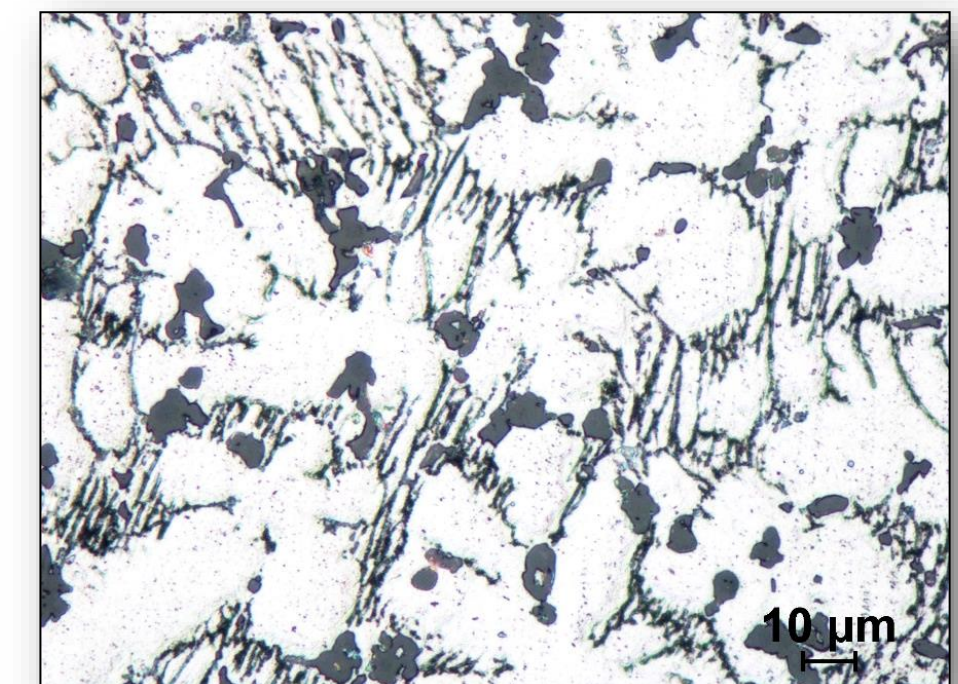
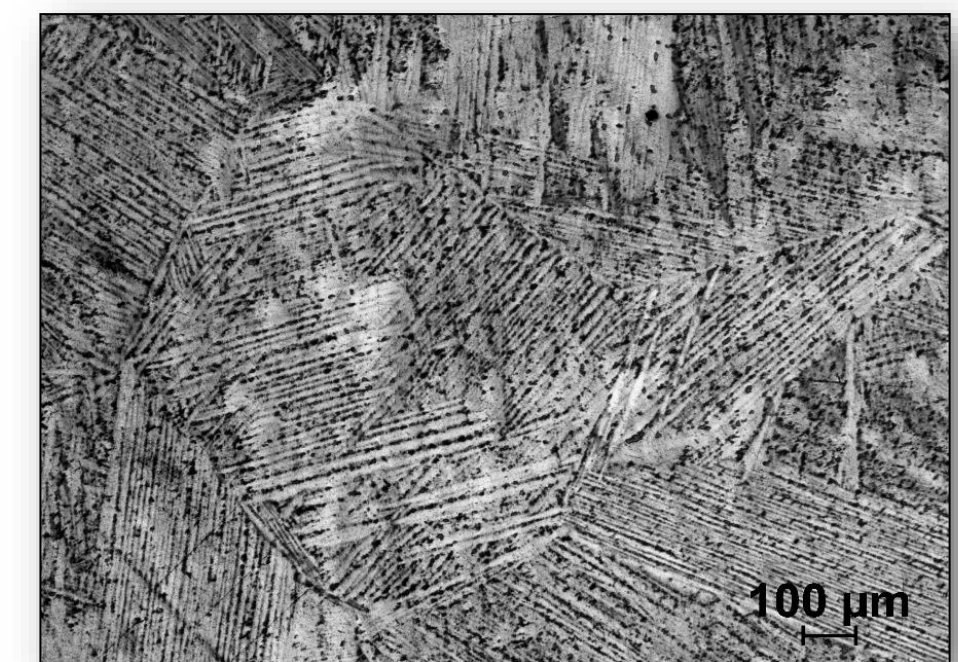
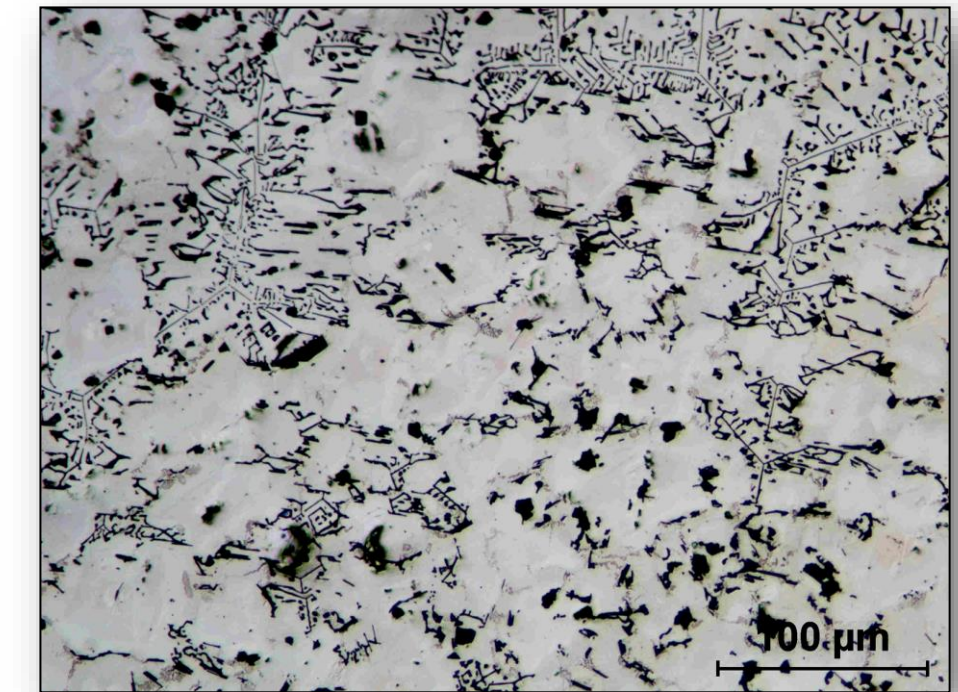
Effect of titanium melting in ceramic crucible

Crucible materials			Elements content, mas. %	
			O	Rest
Bulk crucible	1	Al ₂ O ₃	8.9	Al: 8
	2	MgO	0.69	Mg: 0.26
	3	ZrO ₂ ·Y ₂ O ₃	1.1	Zr: 19.1, Y: 0.13
	4	ZrO ₂ ·Al ₂ O ₃ ·Y ₂ O ₃	5.9	Zr: 9.2, Al: 1.66, Y: 0.038
	5	ZrO ₂ ·MgO	1.2	Zr: 0.93, Mg: 0.001
	6	ZrO ₂ ·TiO ₂	0.3	Zr: 0.06, Y: 0.001, N: 0.7
	7	ZrO ₂ ·MgF ₂	0.16	Zr: 0.036, Mg: 0.001
	8	ZrO ₂ ·Foskor	0.3	Zr: 0.004, Y: 0.001, N: 0.7
	9	ZrO ₂ ·HfO ₂ ·MgO	29.5	Zr: 18.06, Mg: 0.026
	10	ZrO ₂ ·HfO ₂ ·CeO ₂	Intensive reaction during melting	
	11	Y ₂ O ₃ ·ZrO ₂	1.1	Y: 0.013, Zr: 0.3
	12	CaO	2.0	Ca: 0.005
	13	CaO·TiO ₂	0.35	Ca: 0.005
	14	CaO·CaF ₂	0.29	Ca: 0.005
	15	BN(1)	0.08	N: 0.05
	16	BN(2)	0.27	N: 0.02
	17	BN(3)	1.75	N: 0.05
	18	BN·ZrO ₂	0.3	N:0.4
	19	Graphite(1)	0.45	C: 1,53
	20	Graphite(2)	0.32	C: 1.44
	21	Graphite(3)	0.30	C: 1.88
	22	Graphite(4)	0.25	C: 1.87
	23	Graphite(5)	0.22	C:2.23
	24	Isostatic graphite(1)	0.92	C: 1.84
	25	Isostatic graphite(2)	0.37	C: 1.47
	26	Isostatic graphite(3)	0.29	C: 1.7
	27	Isostatic graphite(4)	0.17	C: 1.61
	28	Isostatic graphite(5)	0.39	C: 2.67

Before



After



Effect of Ti-6Al-4V melting in a crucible by VIM



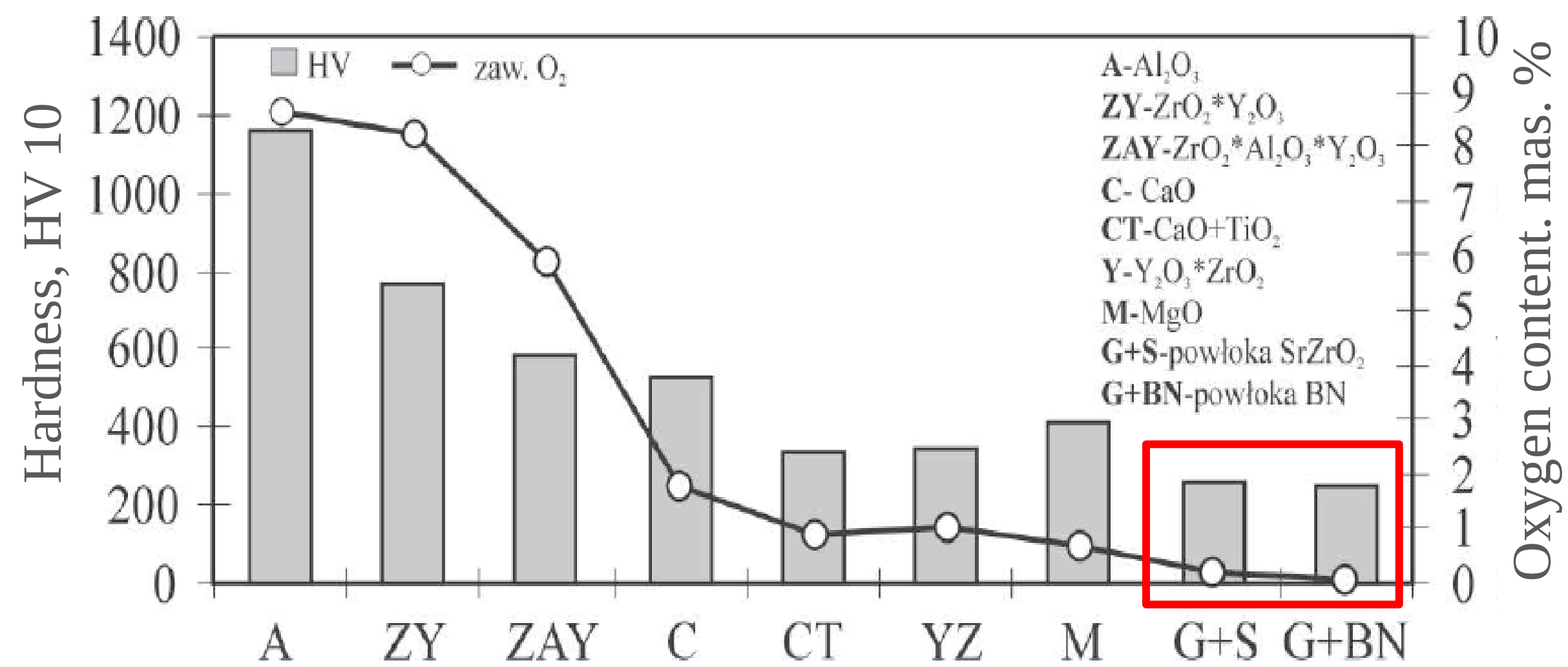
Table 1. Chemical composition of alloy Ti-6Al-4V melted in a crucible in induction furnaces.

Crucible material			Elemental content, [wt.%]			
			O	Al	V	Remainder
Solid crucibles	1	Cu (cold crucible)	0.12	6.11	3.89	C: 0.026
	2	W	0.25	5.94	3.99	W: 27.20
	3	Mo	0.30	5.98	3.27	Mo: 34.90
	4	Ta	0.25	6.08	3.77	Ta: 53.60
	5	BN-ZrO ₂	0.55	5.51	3.86	Zr: 0.76; N: 0.55
	6	Isostatic graphite (1)	0.15	5.81	3.87	C: 1.48
	7	Isostatic graphite (2)	0.15	5.92	4.10	C: 0.71
Plasma-sprayed coatings	8	SiC + SrZrO ₃ (1)	0.82	5.61	3.78	C: 0.63; Zr: 0.81
	9	SiC + SrZrO ₃ (2)	0.32	5.44	3.78	C: 0.76; Zr: 0.14
	10	SiC + SrZrO ₃ (3)	0.29	5.90	3.92	C: 0.74; Zr: 0.03
	11	SiC + ZrO ₂ ·24MgO (1)	0.80	5.97	4.30	C: 0.26; Zr: 1.30; Mg: 0.02
	12	SiC + ZrO ₂ ·24MgO (2)	1.10	5.77	4.19	C: 0.35; Zr: 1.57; Mg: 0.02
	13	SiC + ZrO ₂ ·8Y ₂ O ₃ (1)	0.60	5.72	3.97	C: 0.16; Zr: 1.19; Y: 0.015
	14	SiC + ZrO ₂ ·8Y ₂ O ₃ (2)	0.76	5.67	3.94	C: 0.35; Zr: 1.53; Y: 0.033
	15	SiC + ZrO ₂ ·20Y ₂ O ₃ (1)	0.66	5.80	4.02	C: 0.26; Zr: 0.94; Y: 0.042
	16	SiC + ZrO ₂ ·20Y ₂ O ₃ (2)	0.86	5.66	4.02	C: 0.35; Zr: 1.10; Y: 0.051
	17	SiC + ZrO ₂ ·25CeO·10Y ₂ O ₃ (1)	0.77	5.73	4.30	C: 0.10; Zr: 1.37; Y: 0.023
	18	SiC + ZrO ₂ ·25CeO·10Y ₂ O ₃ (2)	0.90	5.40	3.70	C: 0.29; Zr: 1.47; Y: 0.028
	19	SiC + ZrO ₂ ·5CaO·0.5Al ₂ O ₃ ·0.4SiO ₂ (1)	0.70	6.54	3.79	C: 0.29; Zr: 1.26; Ca: 0.072
Manually applied coatings	20	SiC + ZrO ₂ ·5CaO·0.5Al ₂ O ₃ ·0.4SiO ₂ (2)	1.00	6.12	3.65	C: 0.34; Zr: 1.87; Ca: 0.079
	21	Isostatic graphite + Y ₂ O ₃ + BN + BN (1)	0.12	6.14	3.72	C: 0.74; N: 0.03
	22	Isostatic graphite + Y ₂ O ₃ + BN + BN (2)	0.13	6.07	3.68	C: 0.71; N: 0.02
	23	Isostatic graphite + SrZrO ₃ (1)	0.24	5.66	3.90	C: 0.82; Zr: 0.05; Sr < 0.001
	24	Isostatic graphite + SrZrO ₃ (2)	0.23	5.86	3.81	C: 0.83; Zr: 0.02; Sr < 0.001
	25	SiC + SrZrO ₃ (1)	0.15	5.80	3.80	C: 0.26; Zr: 0.04; Sr < 0.002
	26	SiC + SrZrO ₃ (2)	0.16	5.70	3.63	C: 0.44; Zr: 0.014; Sr < 0.002
	27	SiC + SrZrO ₃ + BN (1)	0.23	5.95	3.63	C: 0.33; Zr: 0.18; Sr < 0.002; N: 0.53
	28	SiC + SrZrO ₃ + BN (2)	0.20	5.70	2.77	C: 0.59; Zr: 0.04; Sr < 0.002; N: 0.60
	29	SiC + MgO + BN	0.70	5.76	3.83	C: 0.42; Mg: 0.11; N: 0.70
	30	SiC + ZrO ₂ + BN	0.34	5.75	3.65	C: 0.34; Zr: 0.47; N: 0.40
	31	SiC + Y ₂ O ₃ + BN	0.25	5.66	3.96	C: 0.25; Y: 0.05; N: 0.28
	32	SiC + BN + Y ₂ O ₃	0.20	5.78	3.89	C: 0.63; N: 0.61; Y: 0.007
	33	SiC + Y ₂ O ₃ + BN + CaF ₂ (1)	0.28	6.05	3.61	C: 0.20; N: 0.29
	34	SiC + Y ₂ O ₃ + BN + CaF ₂ (2)	0.29	6.08	3.64	C: 0.42; N: 0.69
	35	SiC + Y ₂ O ₃ + BN + Y ₂ O ₃ (1)	0.32	5.72	3.41	C: 0.27; N: 0.56
	36	SiC + Y ₂ O ₃ + BN + Y ₂ O ₃ (2)	0.25	6.06	3.50	C: 0.39; N: 0.41
	37	SiC + CaF ₂ + ZrO ₂ + BN	0.17	5.60	3.91	C: 0.22; Zr: 0.01; Ca: 0.001; N: 0.32
	38	SiC + CaF ₂ + BN + Y ₂ O ₃ + BN (1)	0.29	5.97	3.71	C: 0.28; N: 0.53
	39	SiC + CaF ₂ + BN + Y ₂ O ₃ + BN (2)	0.22	6.01	3.07	C: 0.40; N: 0.58

(1), (2) and (3)—adequately first, second and third melt in crucible



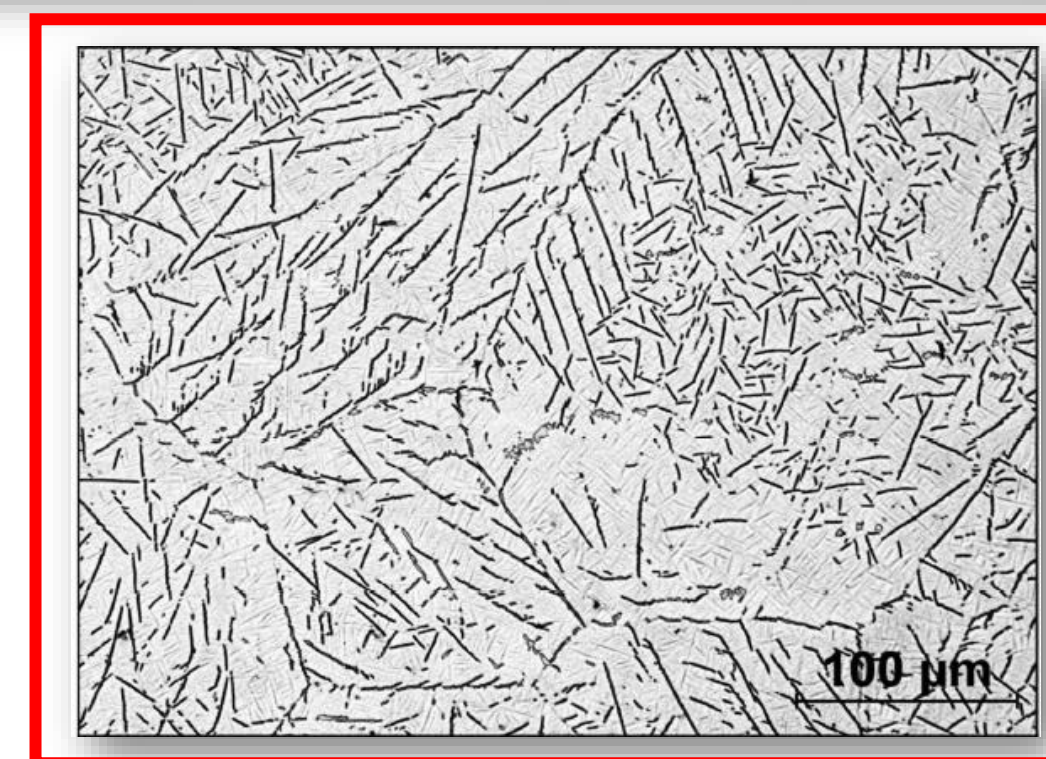
Ti



Crucible materials

Ti-6Al-4V

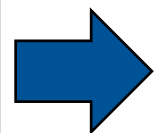
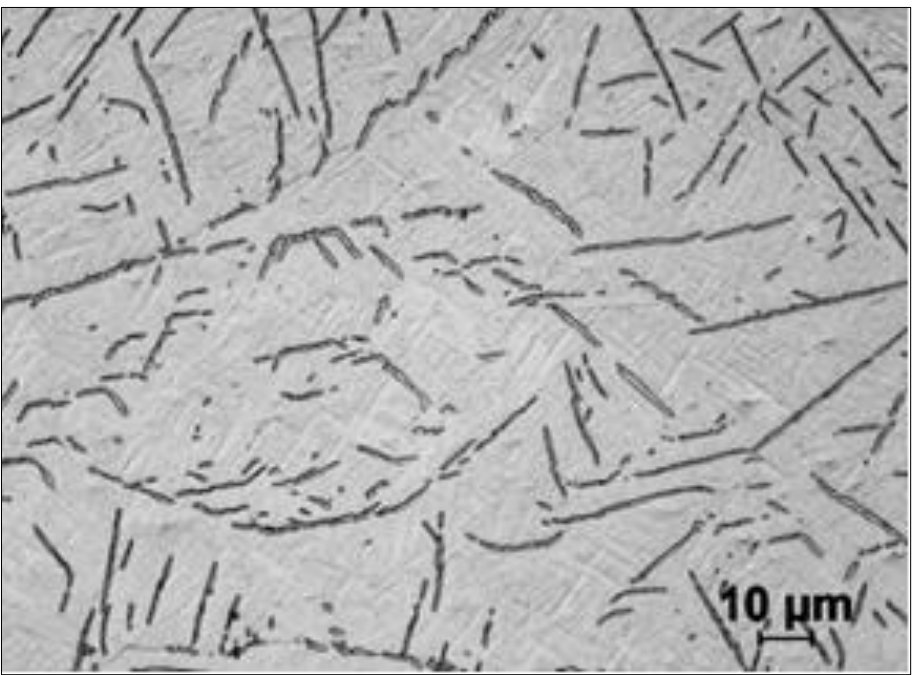
Crucible materials	Element content. mas. %			
	Oxygen	Al	V	Rest
Cu (cold crucible)	0.12	6.11	3.89	C: 0.002
SiC+SrZrO ₃	0.22	5.80	3.63	C: 0.26
SiC+Y ₂ O ₃ +BN+CaF ₂	0.16	5.78	3.89	C: 0.27
Graphite+SrZrO ₃	0.20	5.86	3.81	C: 0.68
Isostatic pressed graphite+Y ₂ O ₃ +BN+BN	0.13	6.07	3.68	C: 0.71; N: 0.02
Isostatic pressed graphite+SrZrO ₃	0.19	5.89	3.95	C: 0.71



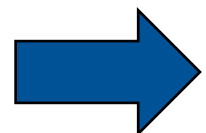
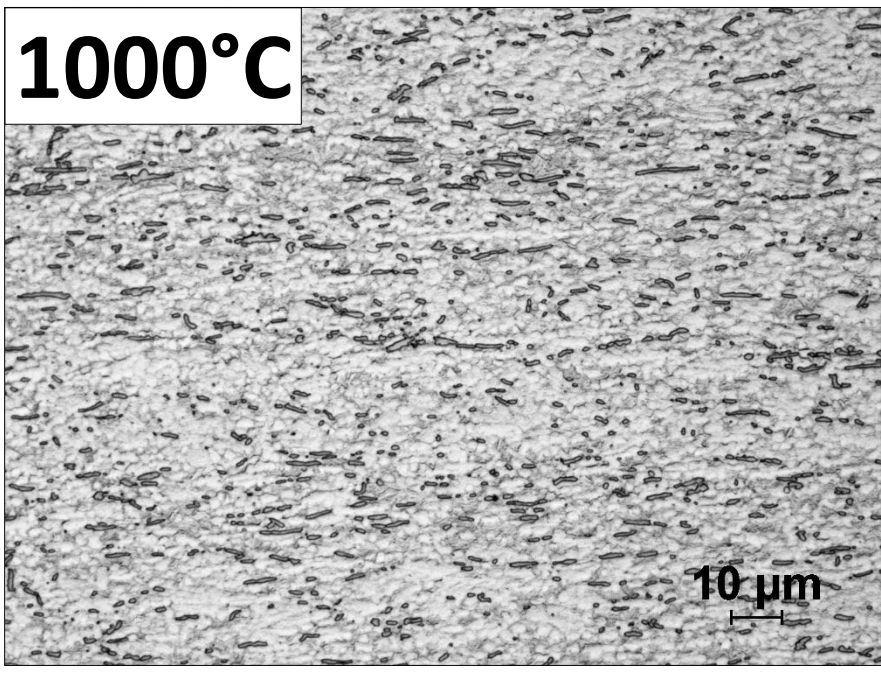
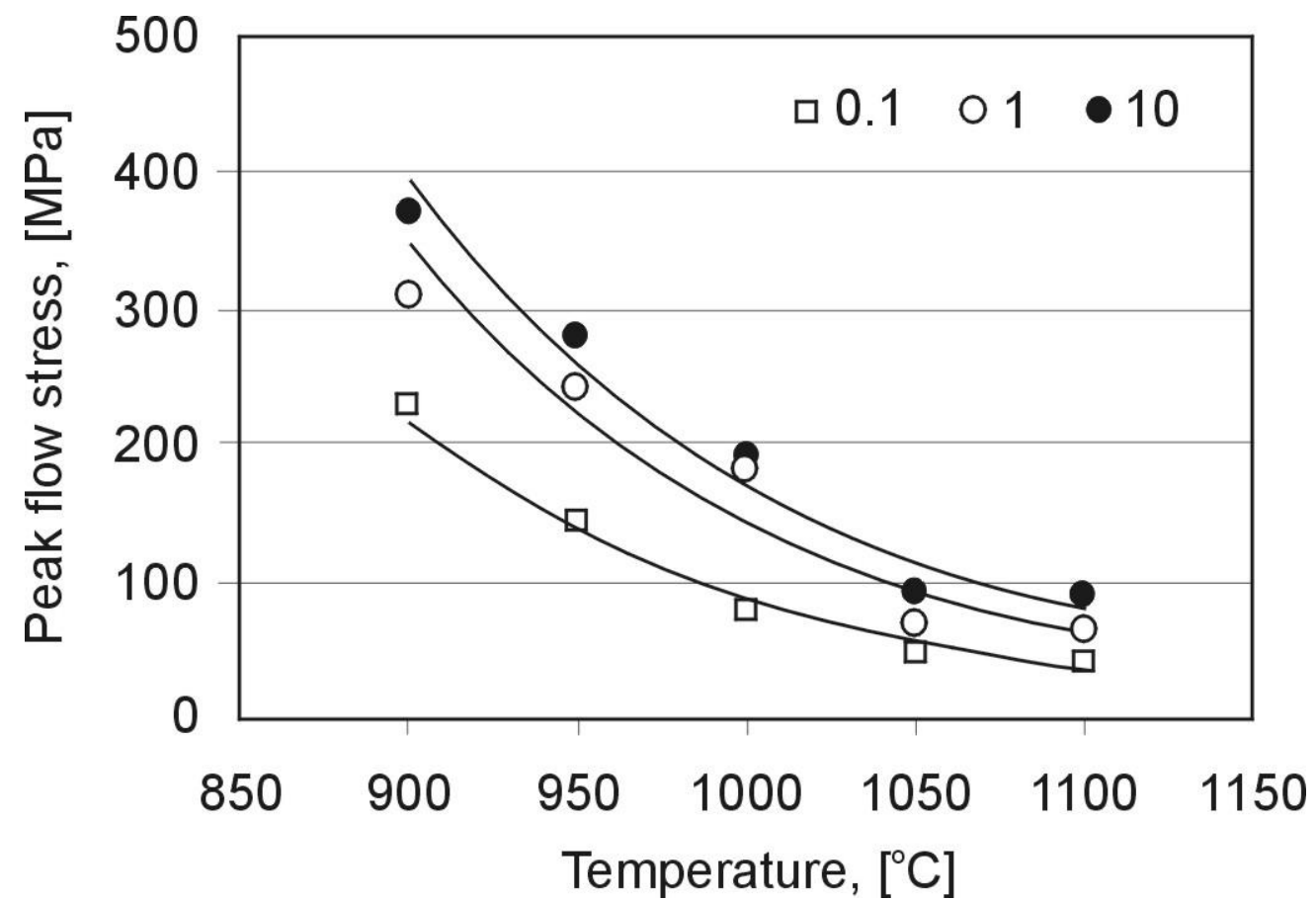
Is it possible to deform?



Deformation of titanium alloys with higher carbon content

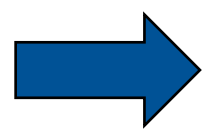


Temperature [°C]	Strain rate [s ⁻¹]		
	0.1	1	10
900			
1000			
1100			



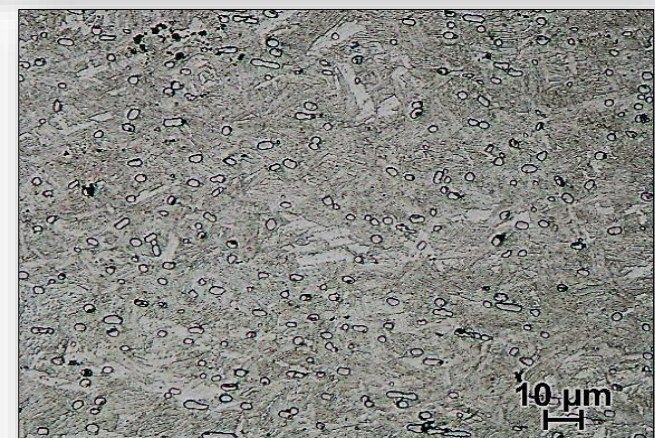
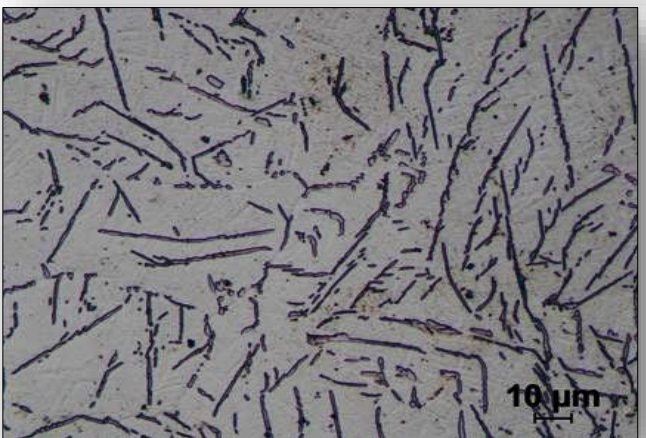
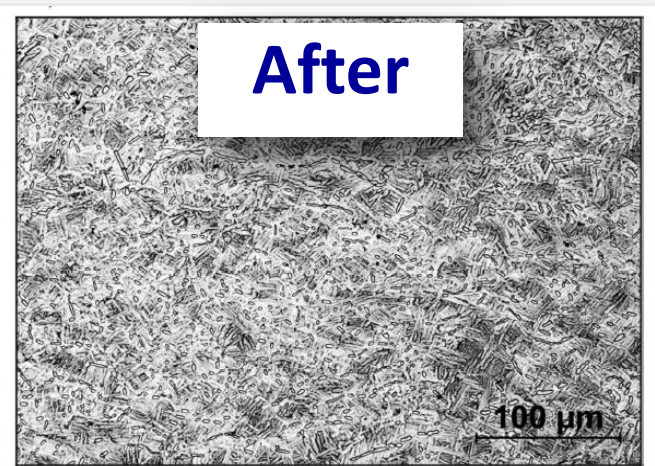
open die forging with elongation

T=1100°C



T=1050°C

shape rolling



Alloy melted in	A _{450°C} %	RA _{450°C} %
	10.6	24
	19.7	40



3. TITANIUM ALUMINIDES MELTED IN GRAPHITE CRUCIBLES



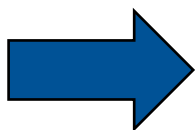
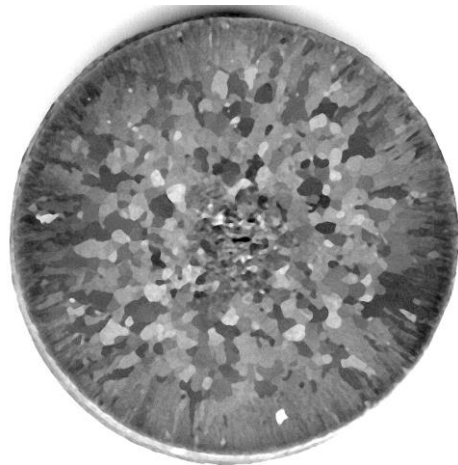
Materials Engineering Forum 30.06.2022

Second generations of TiAl based alloys:

Ti-47Al-2W-0.5Si



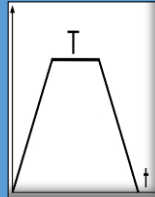
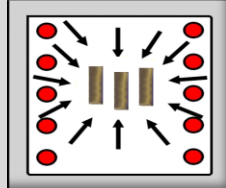
Ti-45Al-8Nb-0.5 (B. C)



Ti-45Al-5Nb-2Cr-1Mo-0.5(B.C)-0.2 Si)



Ti-45Al-8Nb-0,5(B, C) alloy

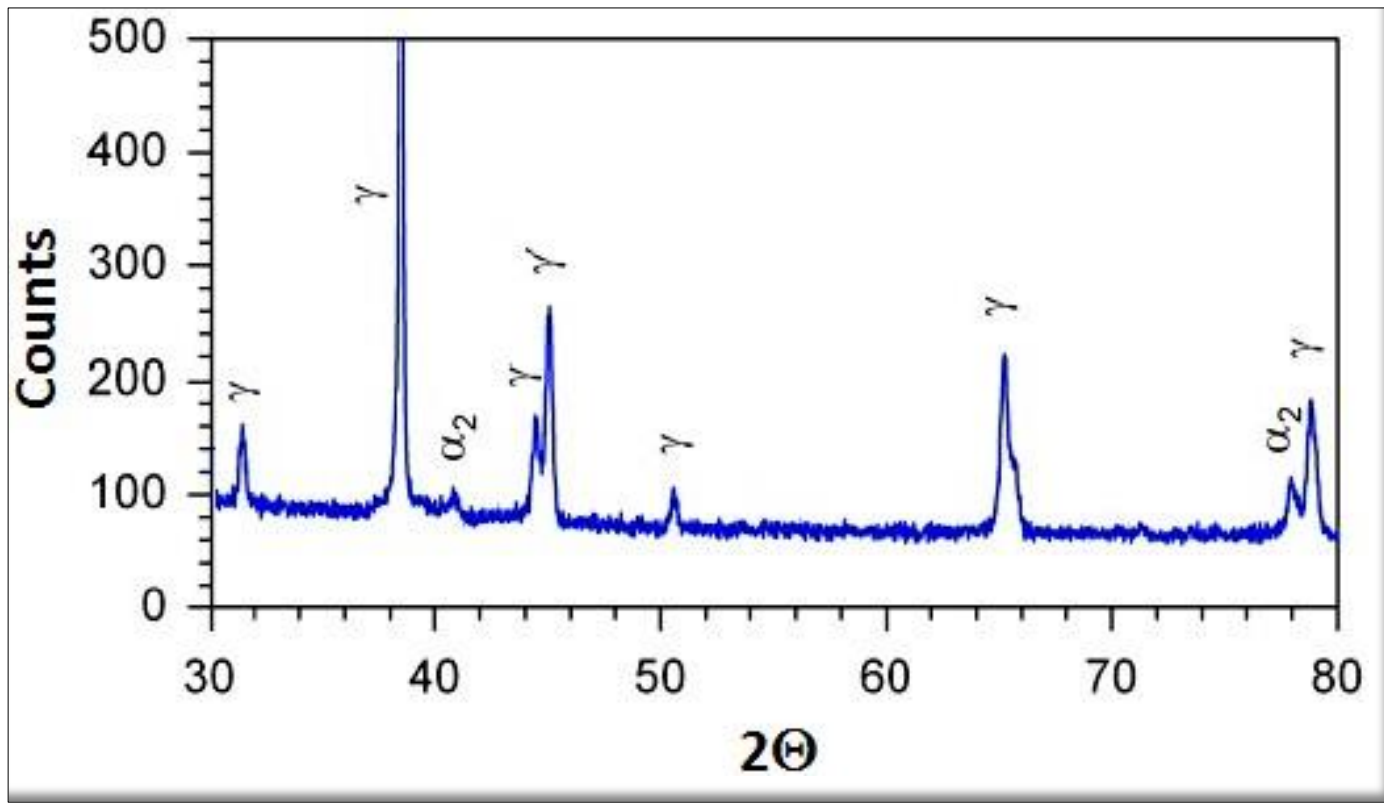
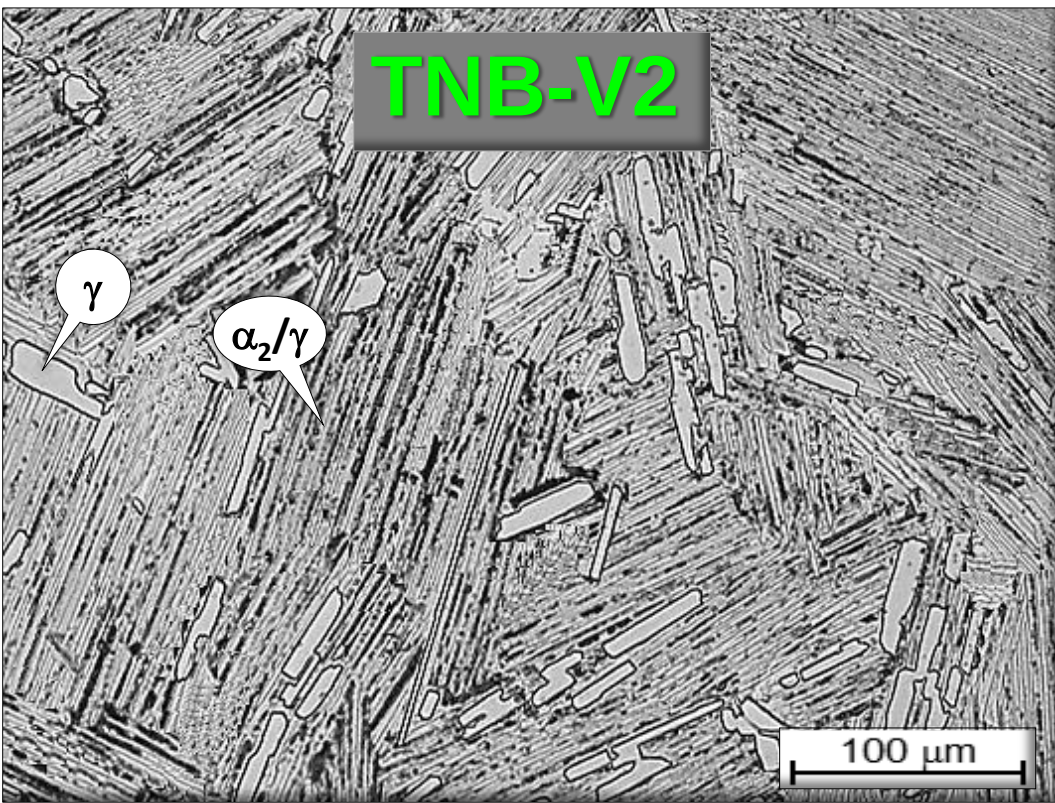
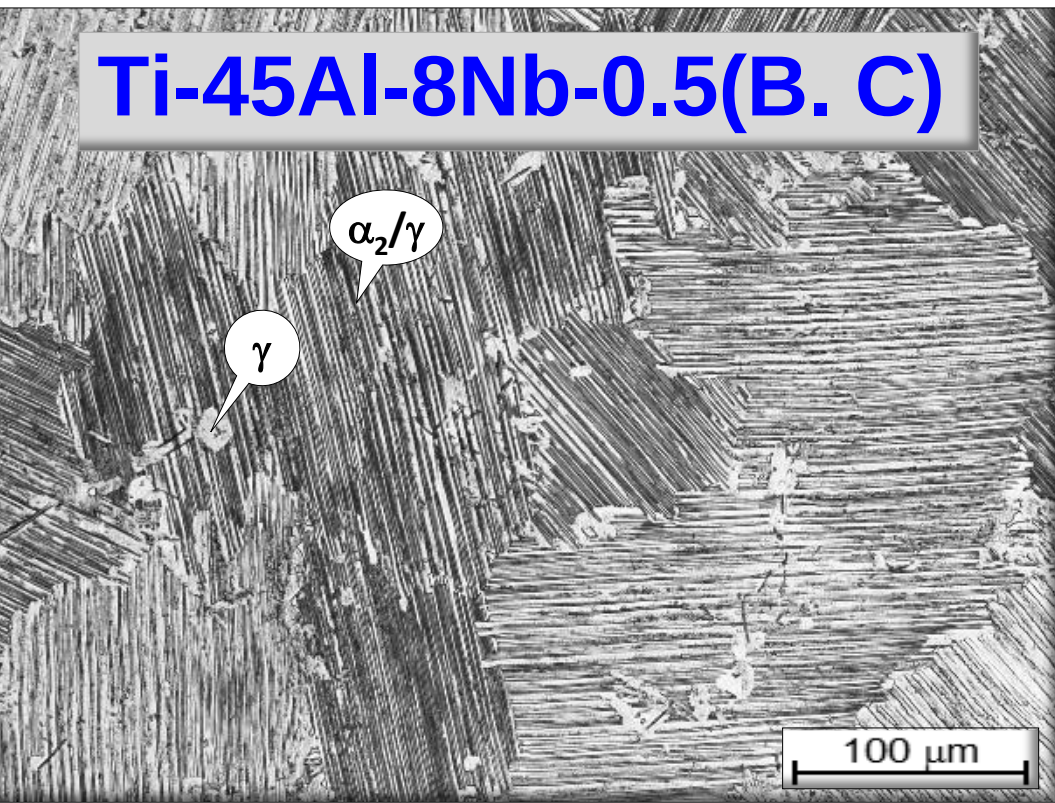
1.	Preparation of a casting moulds		Graphite
2.	Preparation of crucible		Isostatically pressed graphite – 2.0 l
3.	Preparation of feedstock		Al-16Nb + Ti (Grade 2) + C + B
4.	Melting		1650°C/3 min.
5.	Casting to ingot form		Φ55×400 mm 4 kg
6.	Risers removed		
7.	Homogenization		1350°C/1h/furnace cooling
8	Hot isostatic pressing		1260°C/170 MPa/4h
9.	Ingot pre-machined (skinning)		



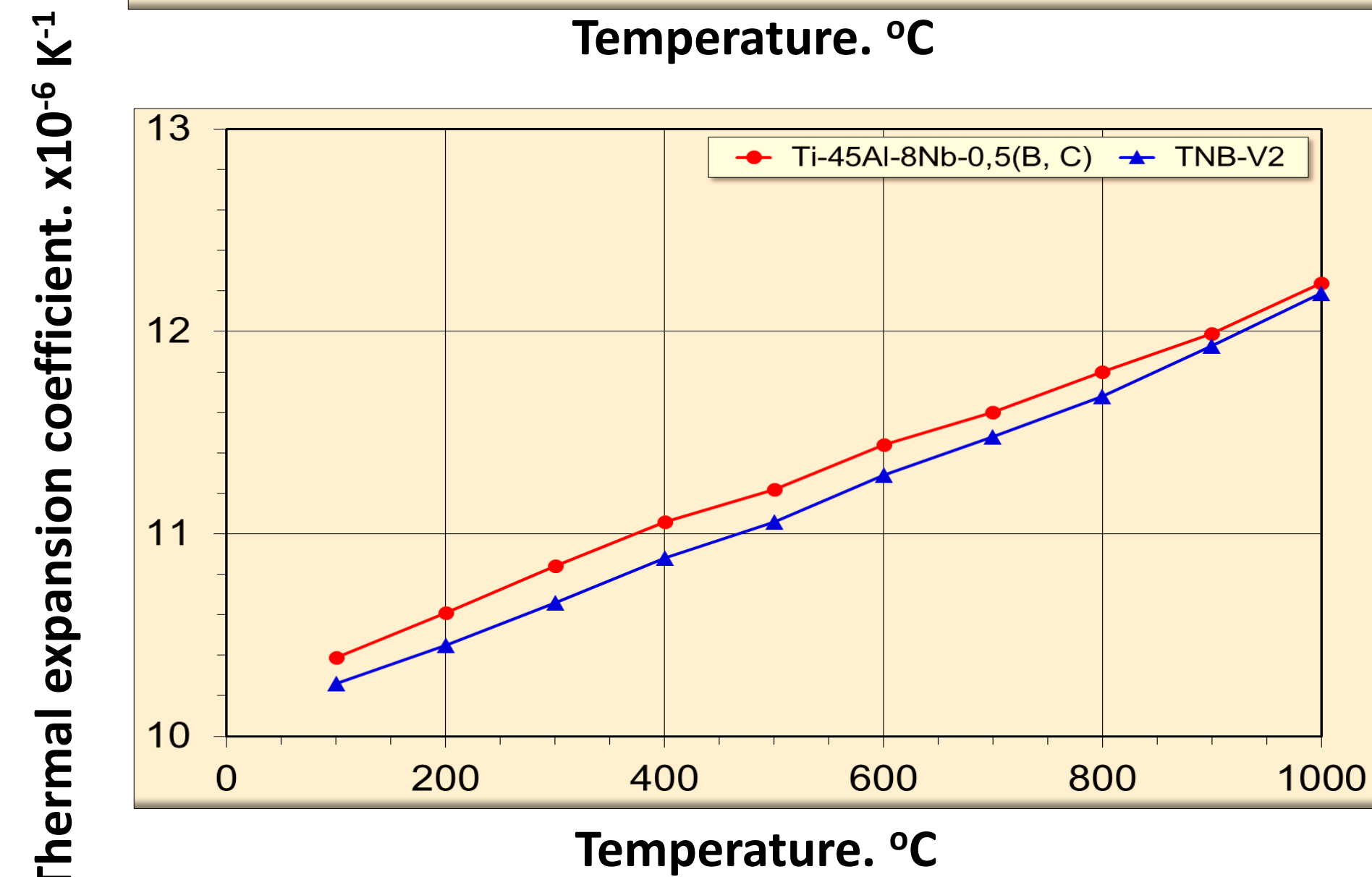
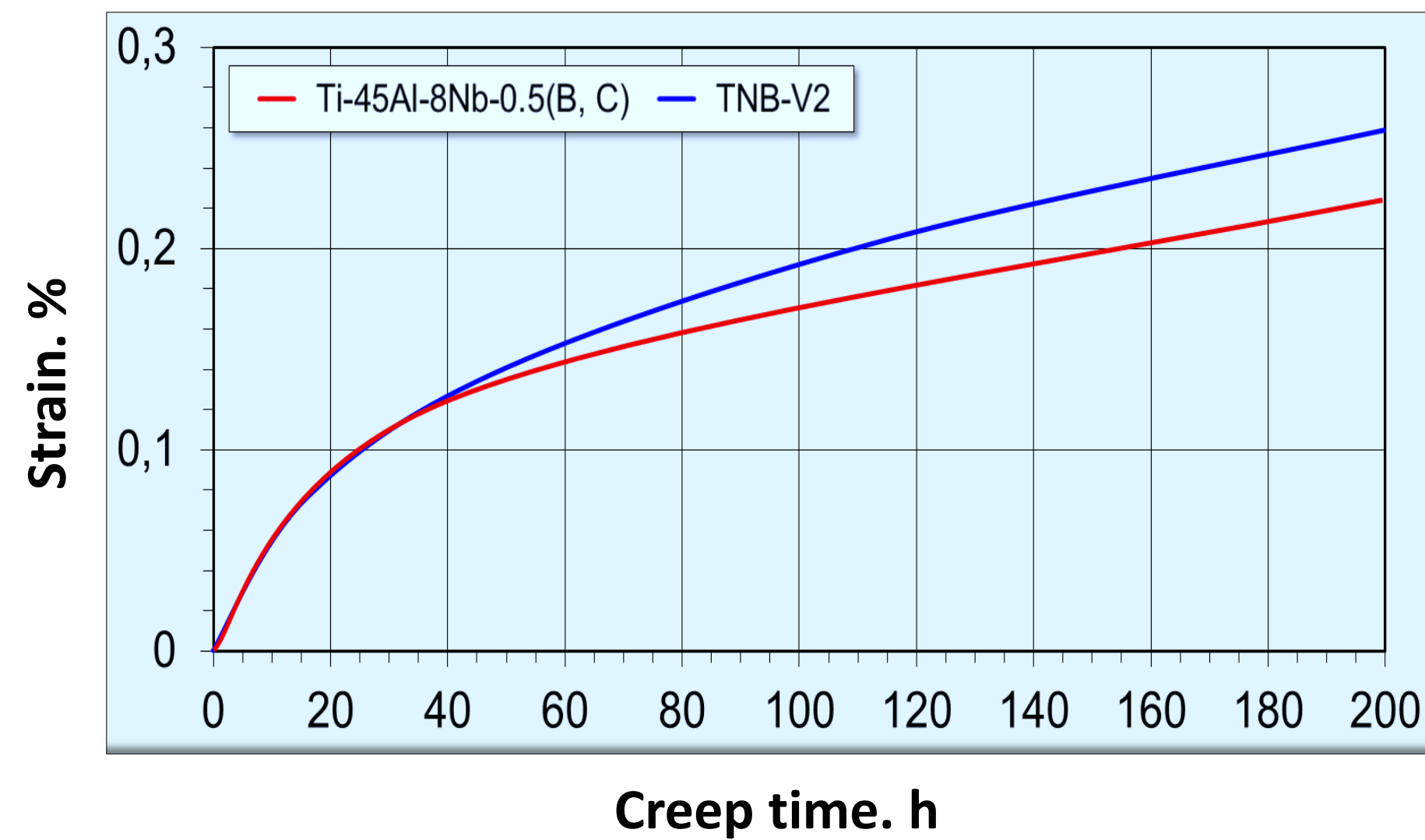
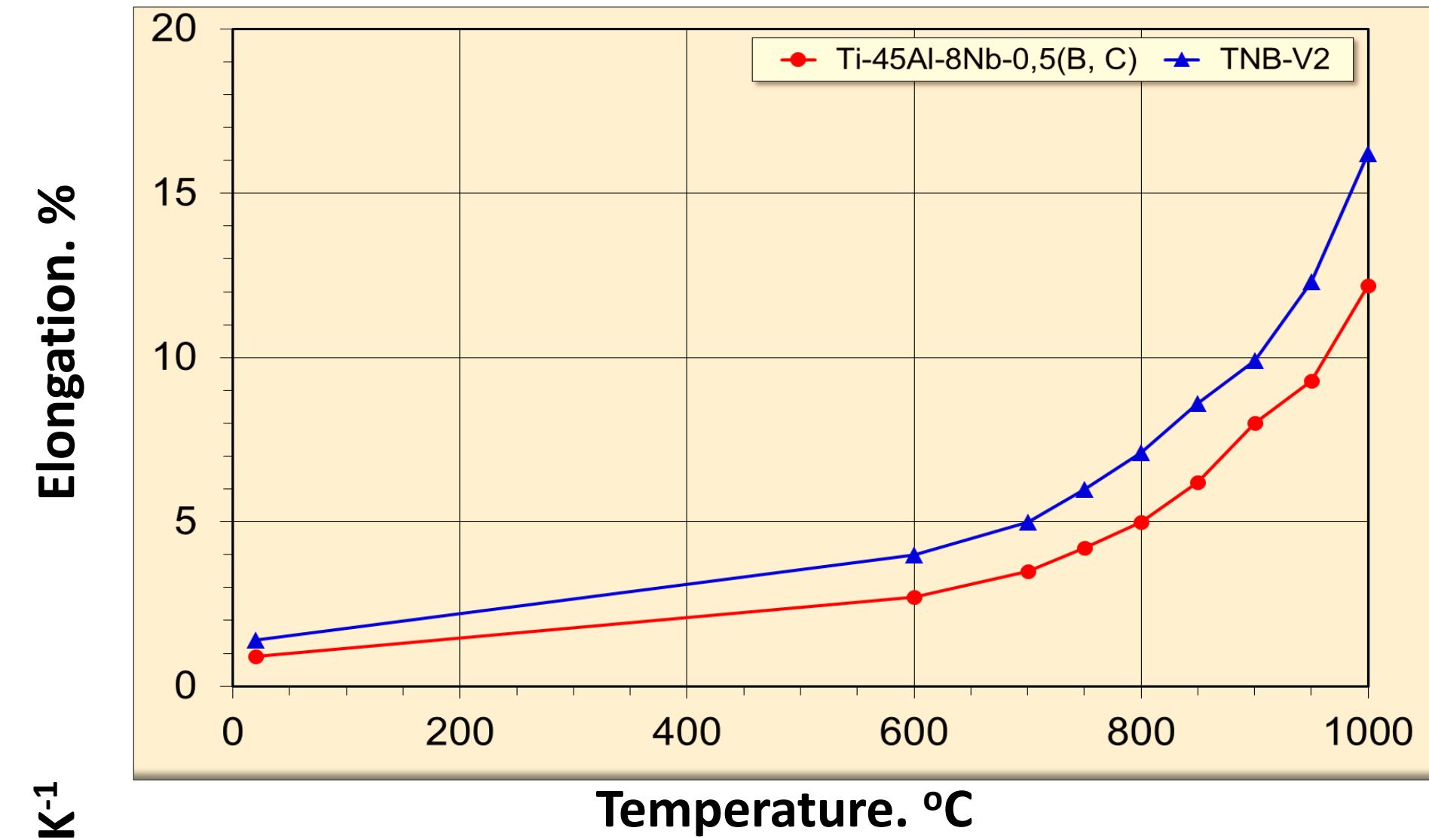
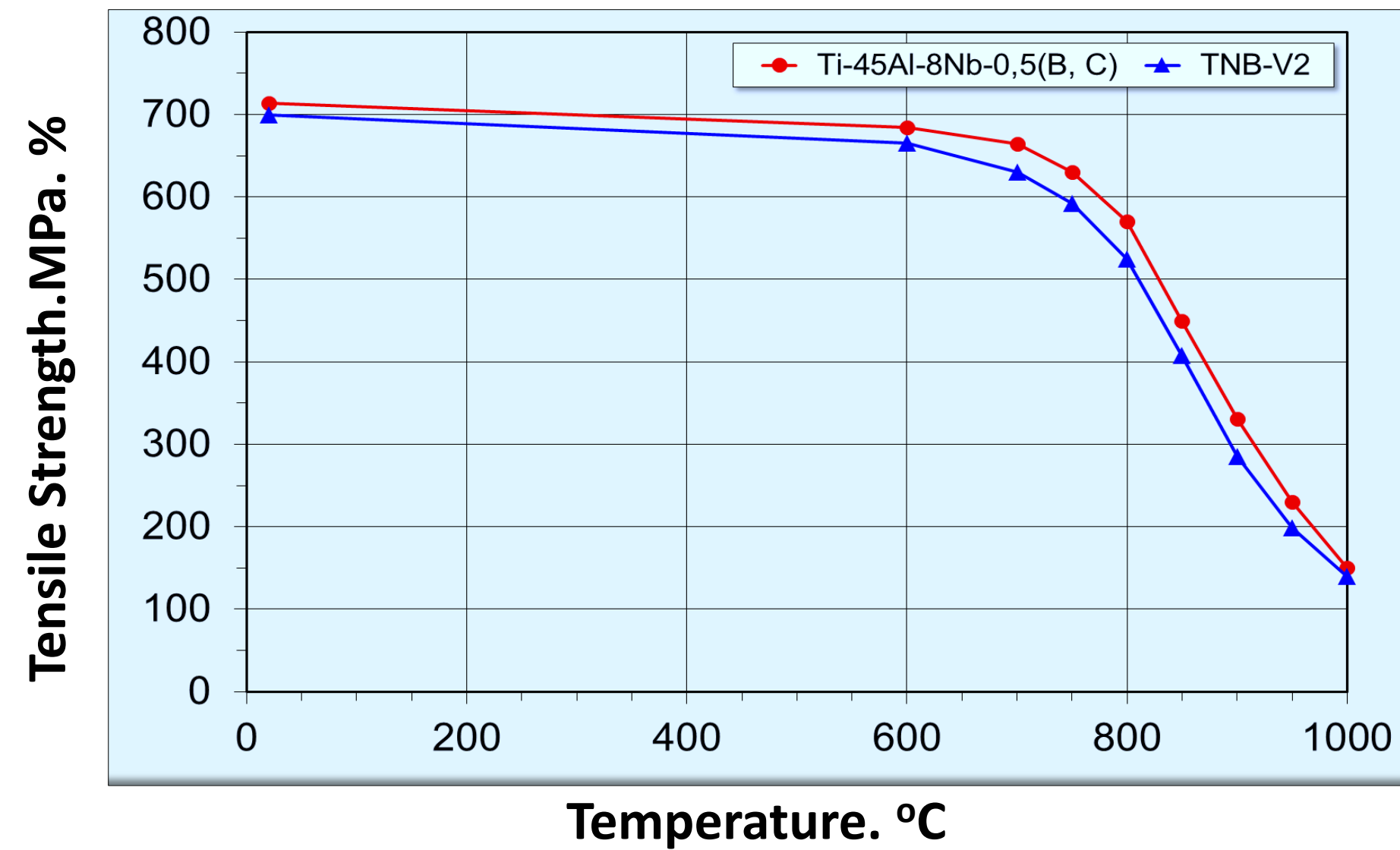
Titanium aluminides melted in special graphite crucibles

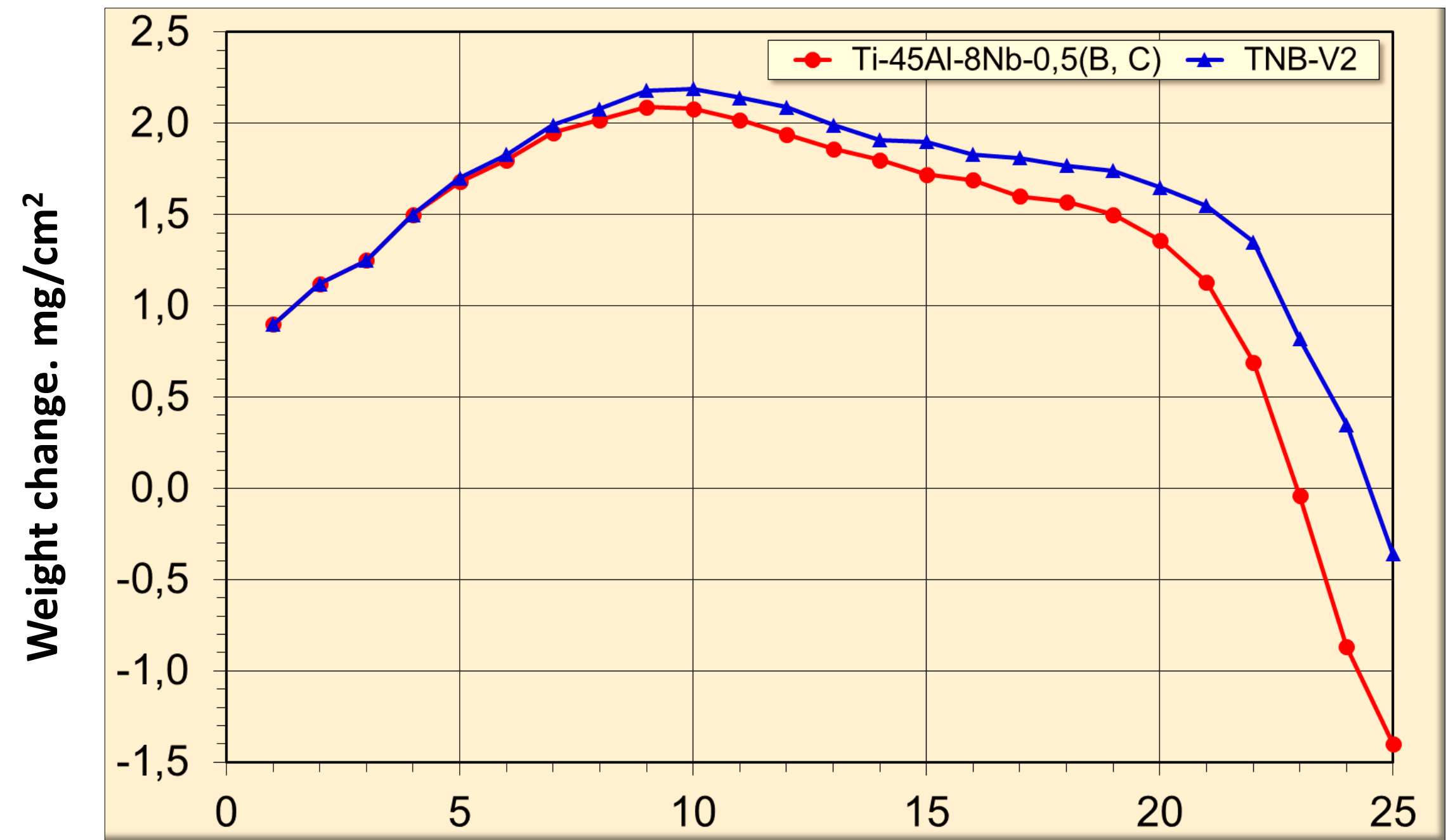


Element	Al	Nb	C	B	O	N	H	Ti
Alloy	at.%				ppm			at.%
Ti-45Al-8Nb-0.5(B. C)	44.25	7.34	0.34	0.15	935	96	17	Rest
TNB-V2	45.40	8.10	0.20	0.20	800	100	30	

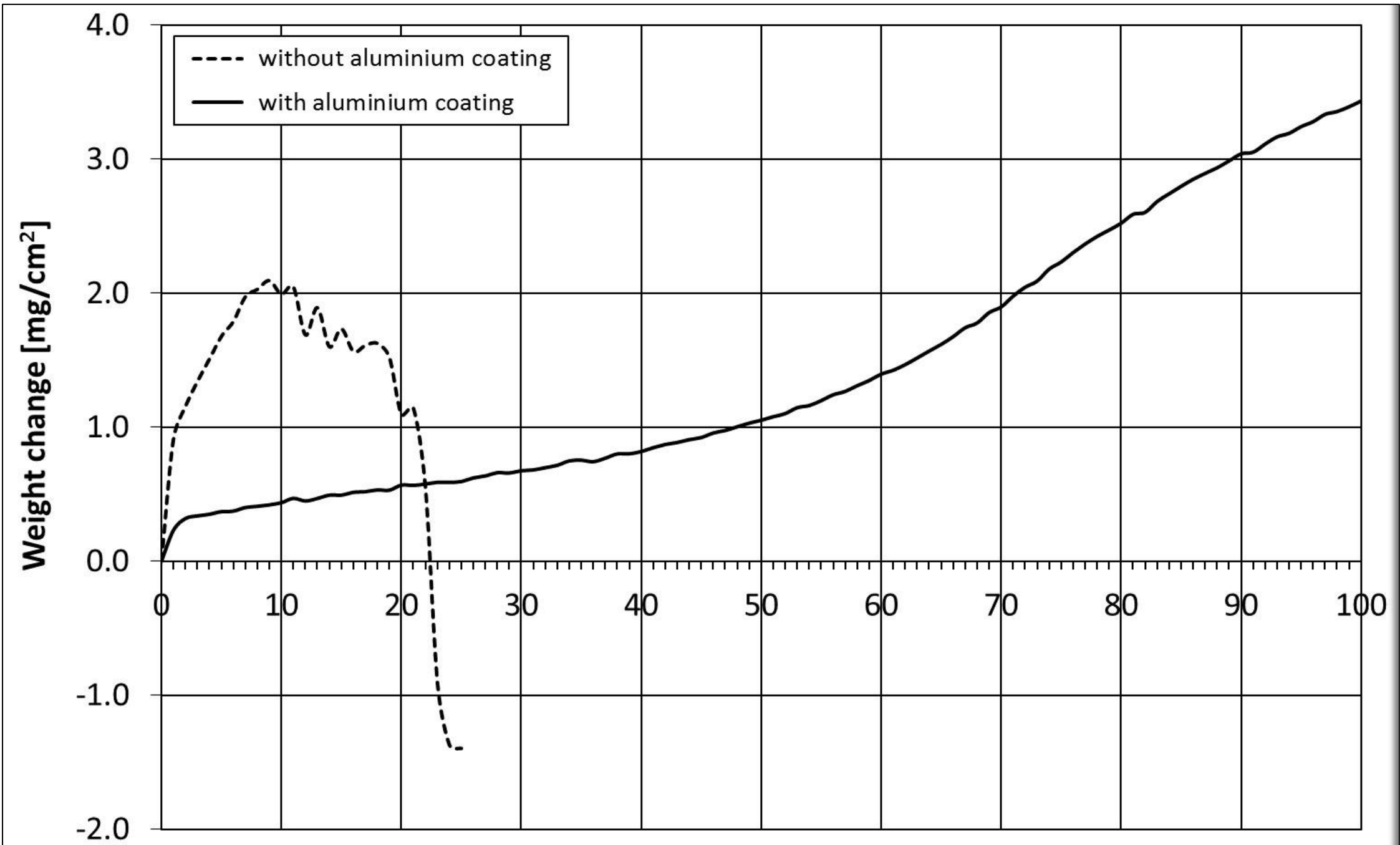


Properties of Ti-45Al-8Nb-0.5(B, C) – SUMMARY





No. of cycles. oxidation at temperature 950°C



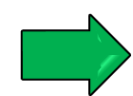
No. of 23-h cycles at 950°C

Alloy	λ	UTS	YS	EL	E	Creep resistance	Oxidation resistance
Ti-45Al-8Nb-0.5(B, C)							
TNB-V2							

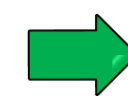


Manufacturing of blades (Ti-47Al-2W-0.5Si alloy)

Preparation of ceramic shell mould



Alloy production

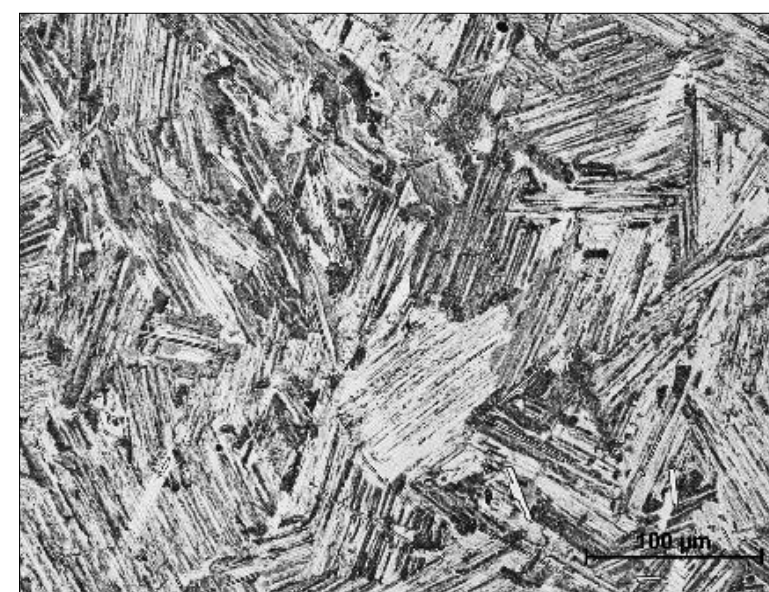
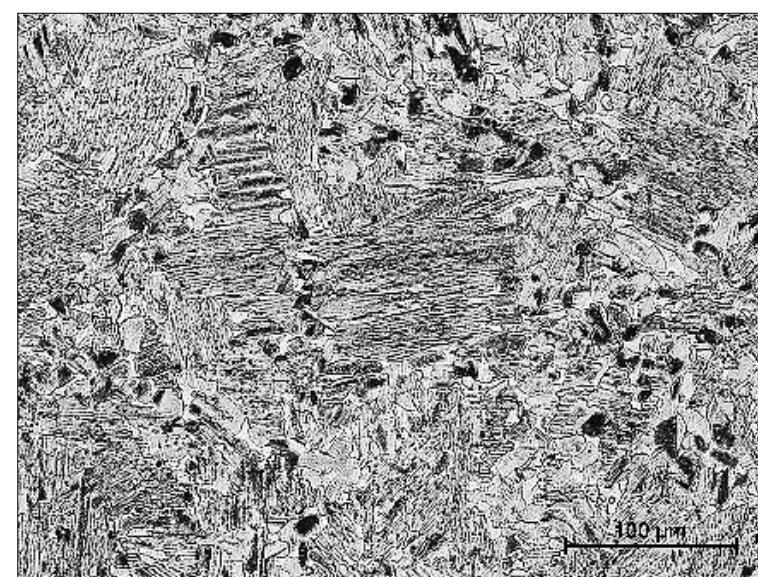
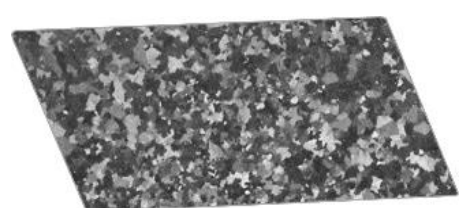
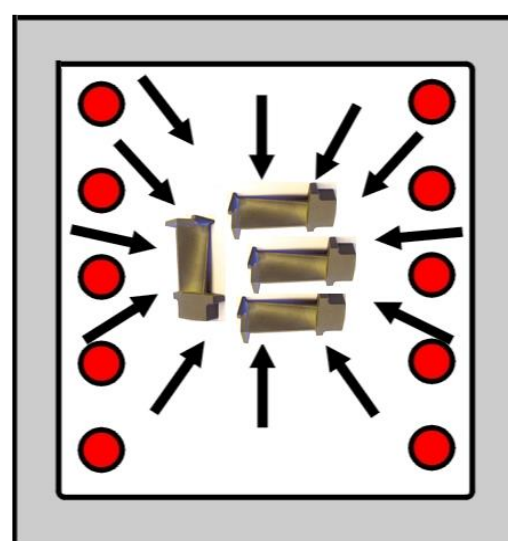


Melting and casting

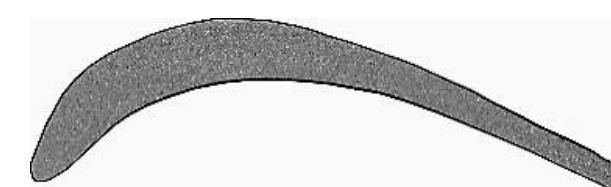
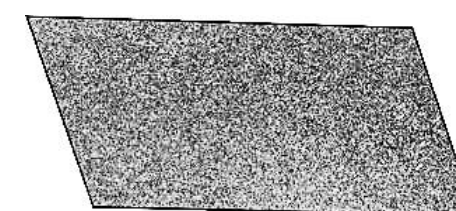
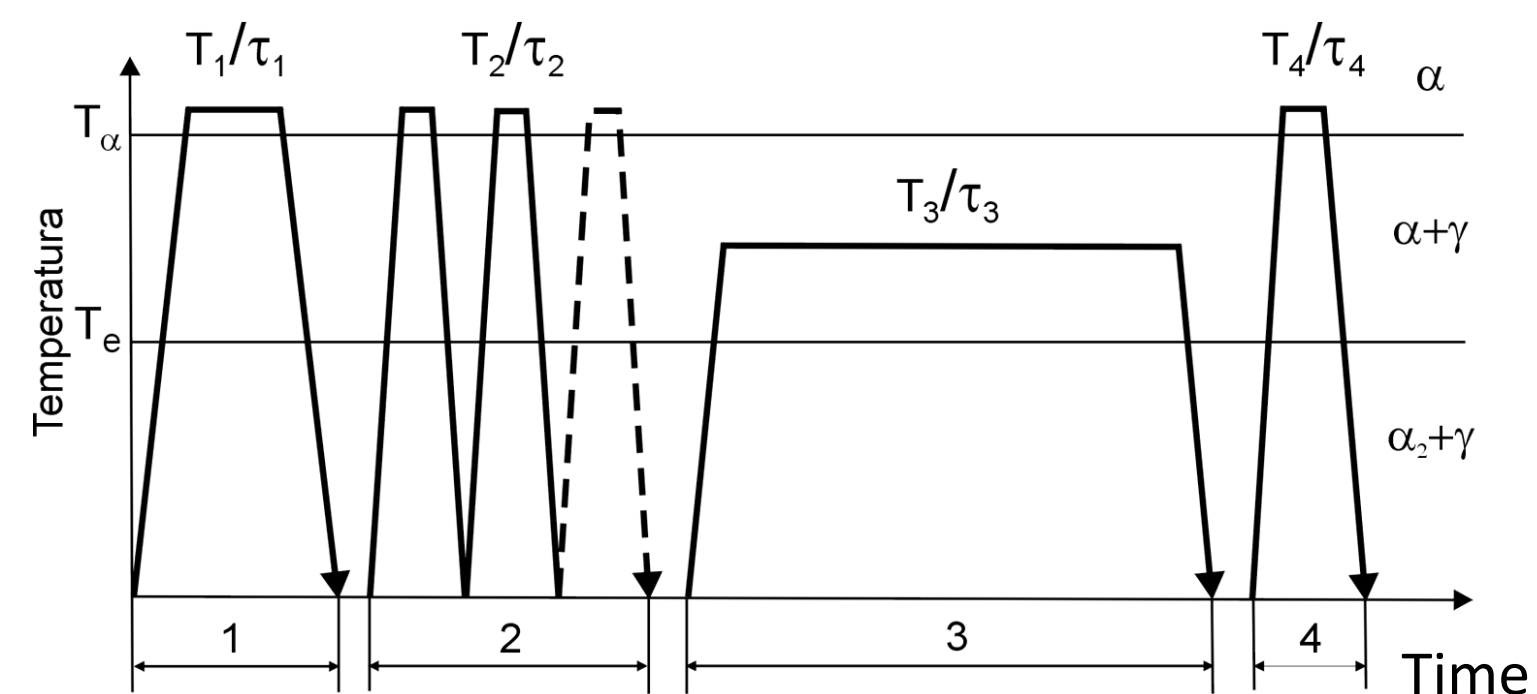


Final treatment

Hot isostatic pressing



Special heat treatment



Machining and surface treatment



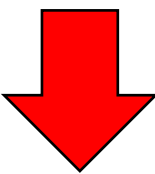
4. TITANIUM ALLOYS WITH CARBON



Materials Engineering Forum 30.06.2022

Alloy	Max. content of impurities. mas. %			
	O	N	H	C
Commerially pure titanium				
Ti Grade 1	0.18	0.03	0.015	0.08
Ti Grade 2	0.25	0.03	0.015	0.08
Ti Grade 3	0.35	0.05	0.015	0.08
Ti Grade 4	0.40	0.05	0.015	0.08
Ti-0.2Pd	0.25	0.03	0.015	0.08
α and near- α alloys				
Ti-5Al-2.5Sn	0.20	0.05	0.020	0.08
Ti-5Al-2.5Sn-ELI	0.12	0.07	0.012	0.08
Ti-8Al-1Mo-1V	0.12	0.05	0.015	0.08
Ti-6Al-2Sn-4Zr-2Mo	0.15	0.05	0.012	0.05
Ti-6Al-2Nb-1Ta-0.8Mo	0.10	0.02	0.012	0.03
Ti-2.25Al-11Sn-5Zr-1Mo	0.17	0.04	0.008	0.04
Ti-5.8Al-4Sn-3.5Zr-0.7Nb-0.5Mo-0.35Si	0.15	0.03	0.006	0.08
$\alpha+\beta$ alloys				
Ti-6Al-4V	0.20	0.05	0.012	0.10
Ti-6Al-4V-ELI	0.13	0.05	0.012	0.08
Ti-6Al-6V-2Sn	0.20	0.04	0.015	0.05
Ti-6Al-2Sn-4Zr-6Mo	0.15	0.04	0.012	0.04
Ti-5Al-2Sn-2Zr-4Mo-4 Cr	0.14	0.04	0.012	0.05
Ti-3Al-2.5V	0.12	0.02	0.015	0.05
Ti-4Al-4Mo-2Sn-0.25Si	0.12	0.05	0.012	0.02
near- β and β alloys				
Ti-15Mo	0.20	0.05	0.015	0.10
Ti-13V-11Cr-3Al	0.17	0.05	0.015	0.05
Ti-10V-2Fe-3Al	0.13	0.05	0.015	0.05
T-15Mo-3Nb-3Al-0.2Si	0.17	0.05	0.015	0.05
Ti-35V-15Cr	0.08	0.05	0.015	0.05

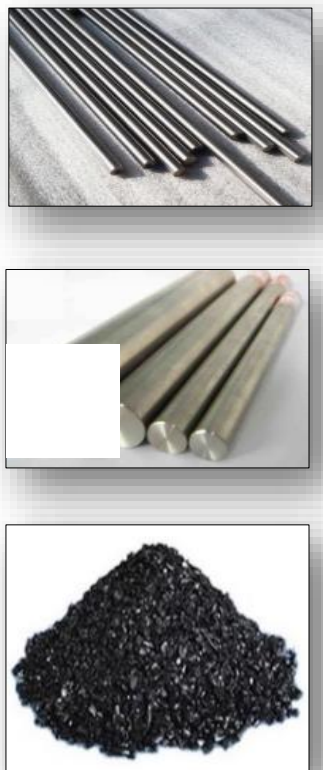
high alloy purity



problem with obtaining high strength



Feedstock

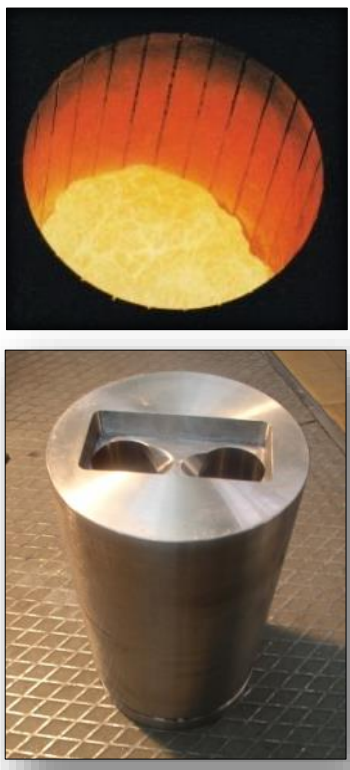


Melting



Institut Für Elektroprozesstechnik
Leibniz Universität Hannover

Casting



Ingot



Homogenization



Hot rolling



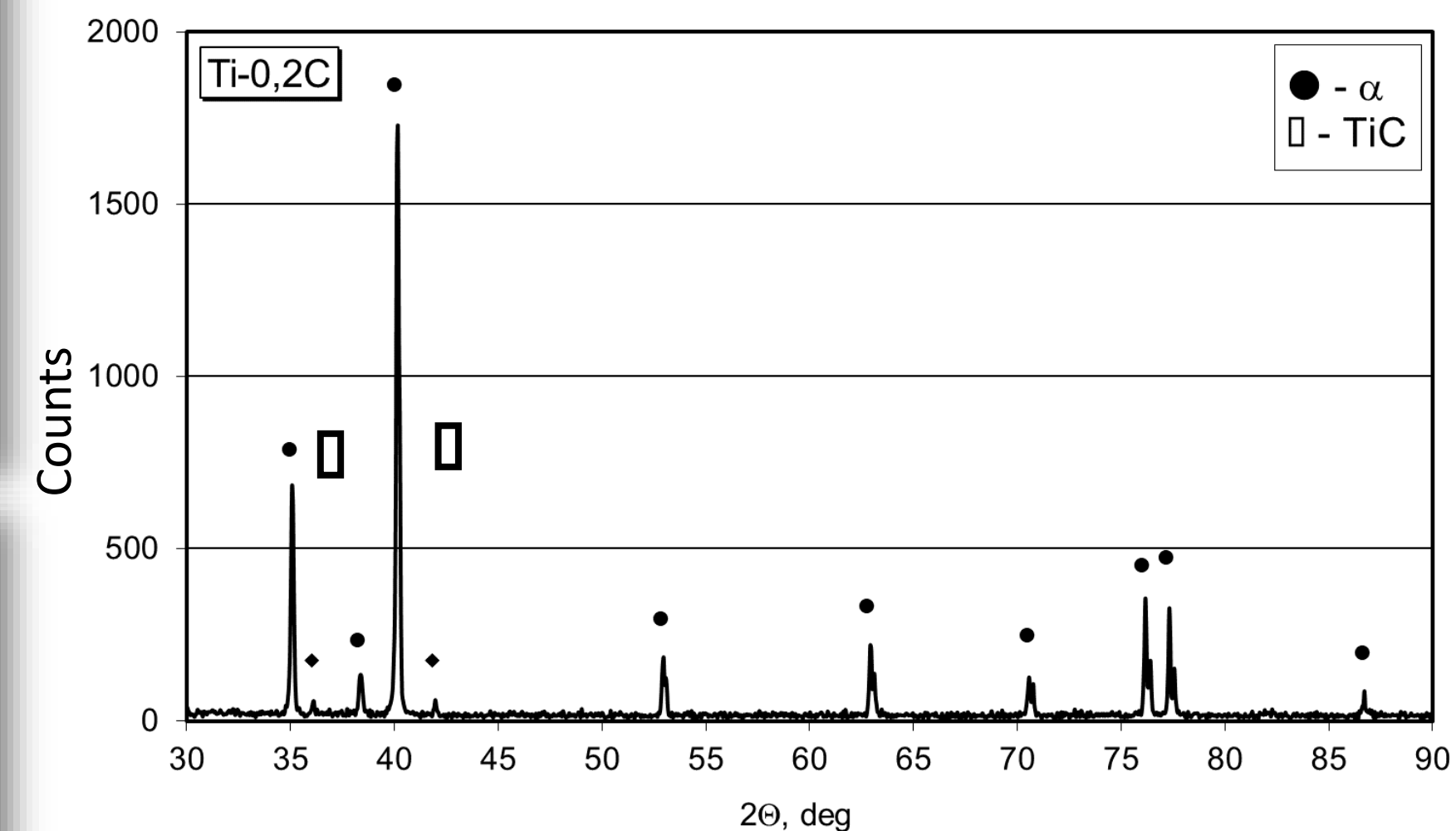
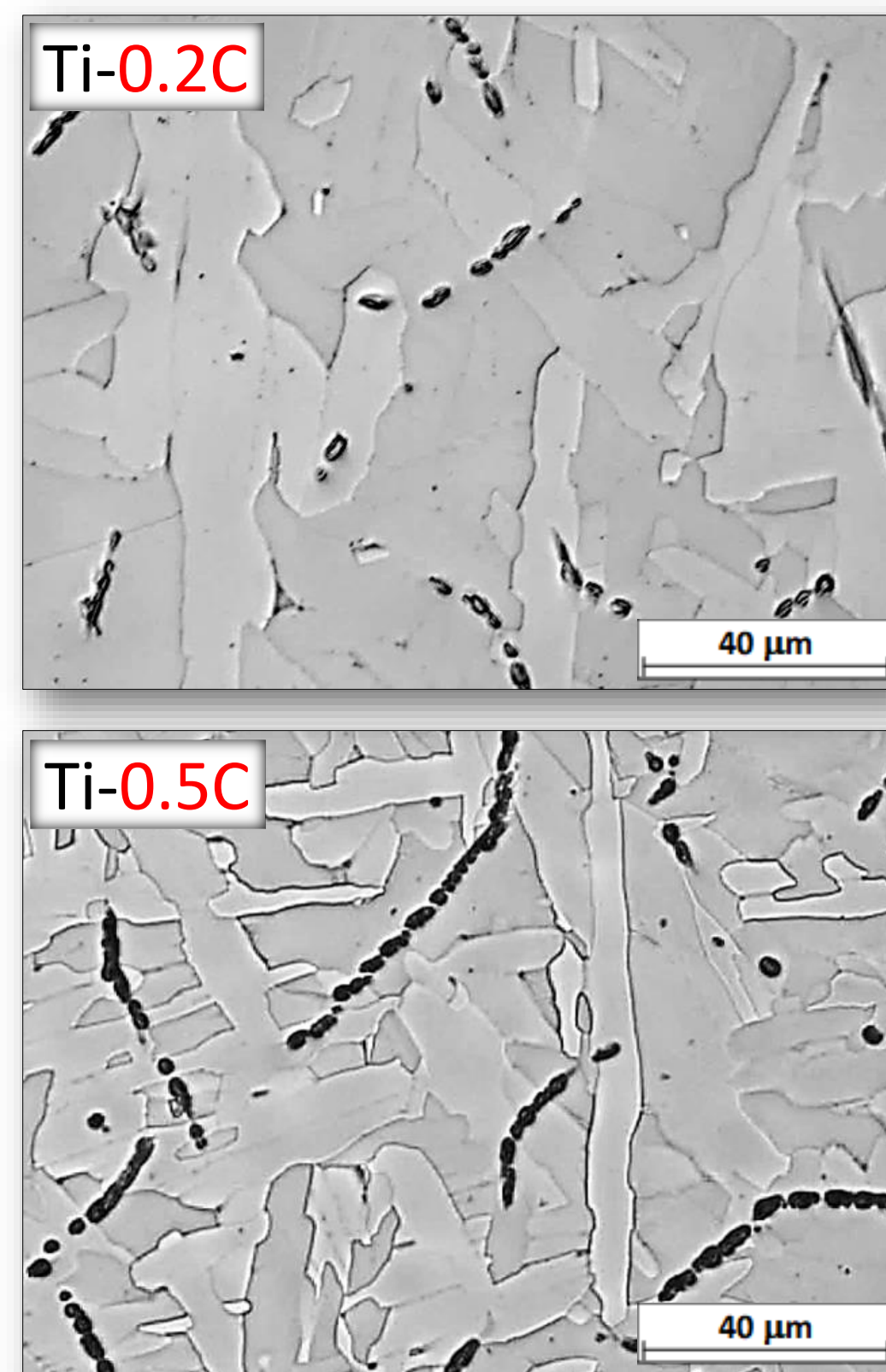
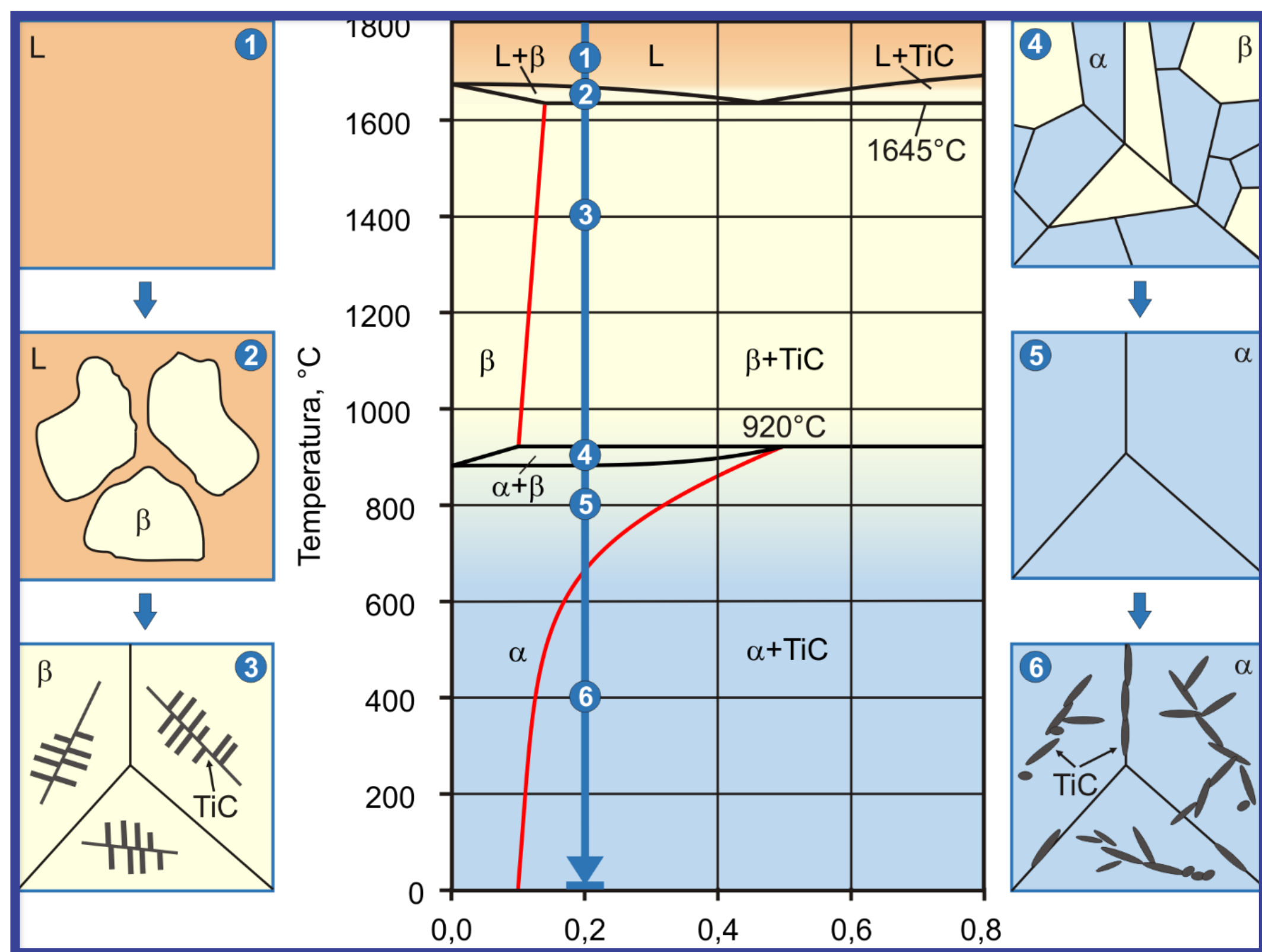
Bergakademie Freiberg

Rods



Heat treatment



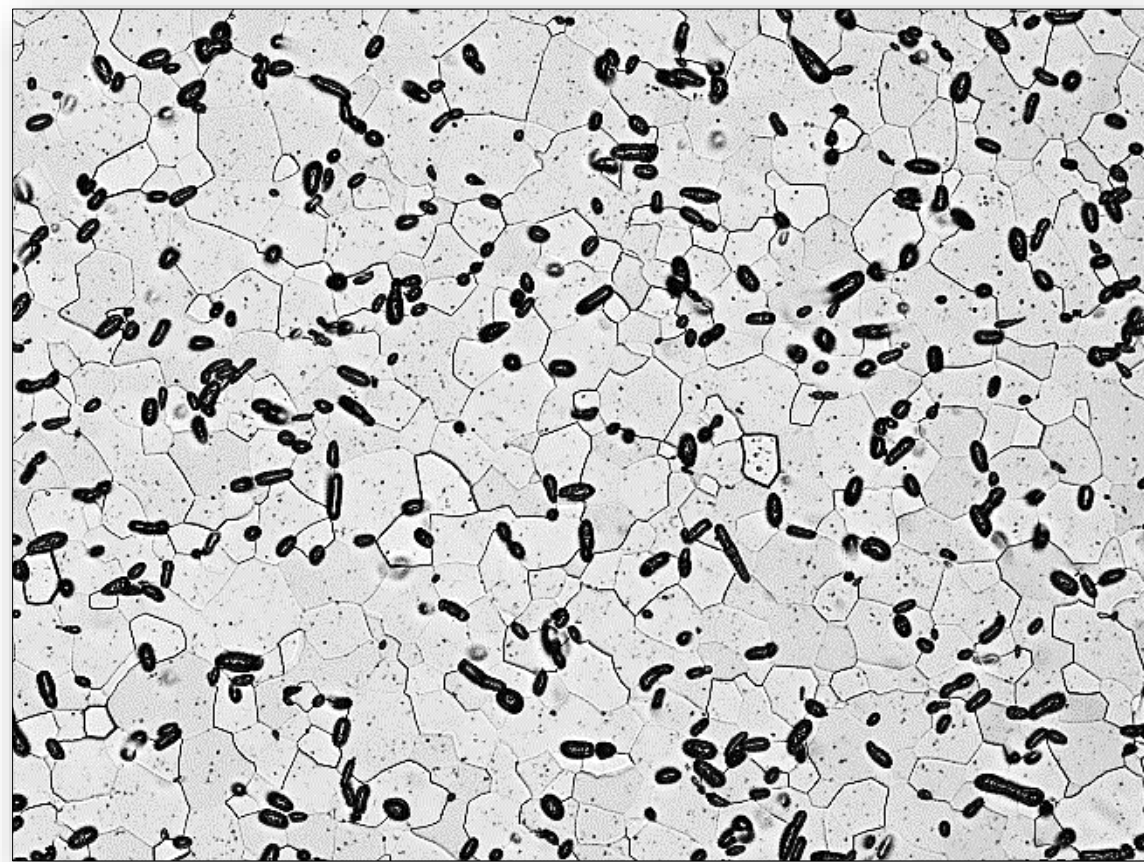
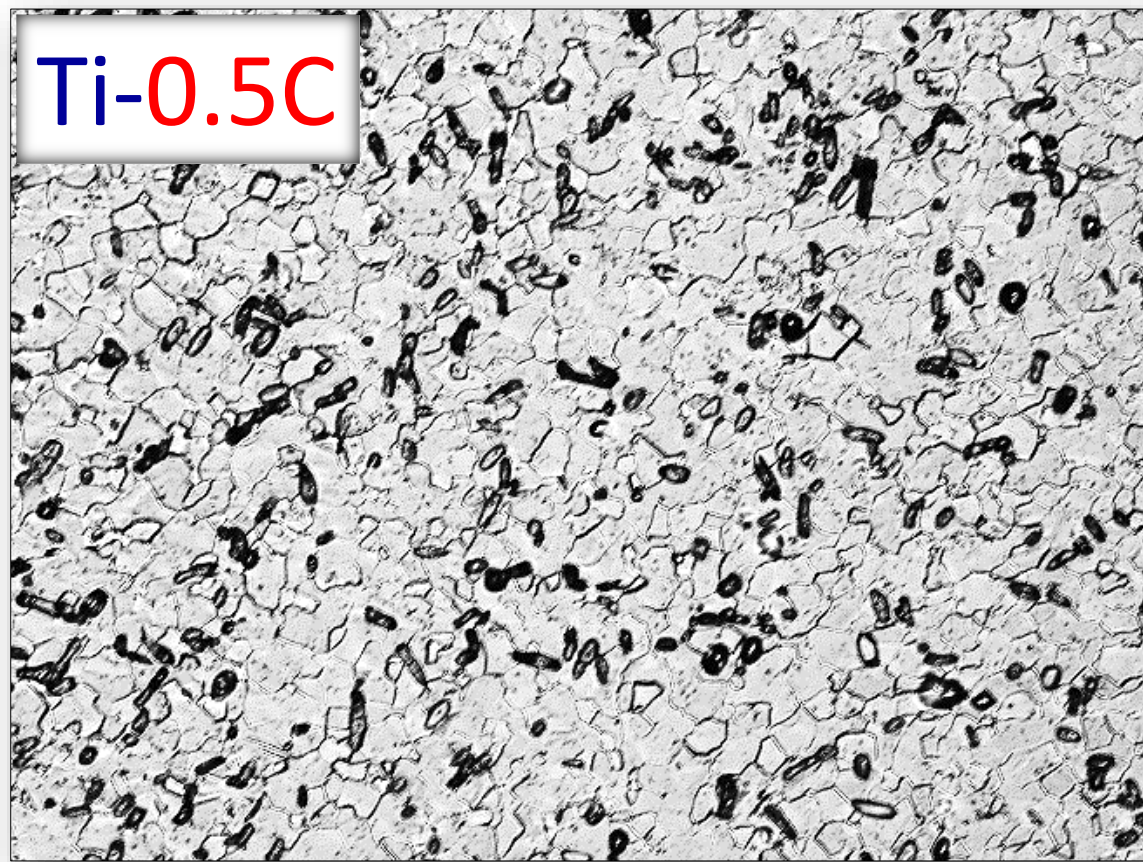
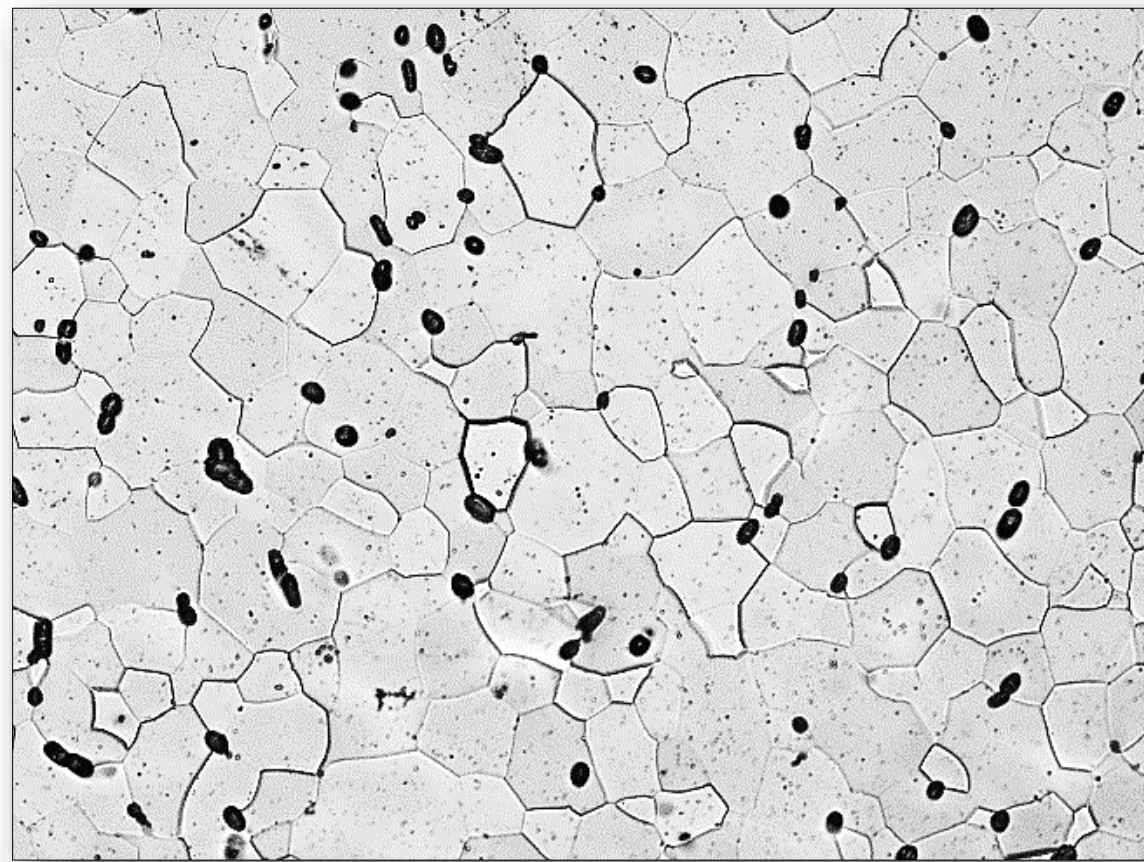
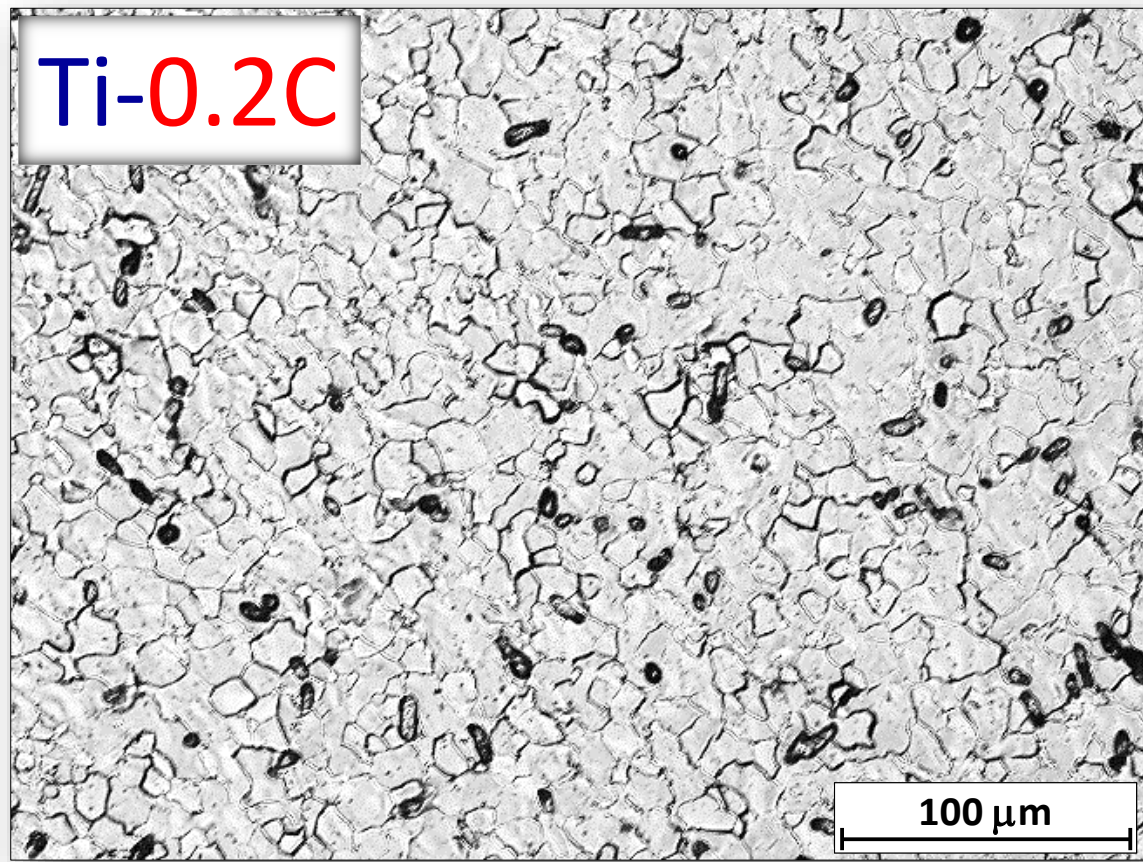


Under phase equilibrium conditions the processes of microstructure formation follows the sequence:

0.0%C ➡ $L \rightarrow \beta \rightarrow \alpha$

0.2%C ➡ $L \rightarrow \beta + L \rightarrow \beta + \text{TiC} \rightarrow \alpha + \beta \rightarrow \alpha \rightarrow \alpha + \text{TiC}$

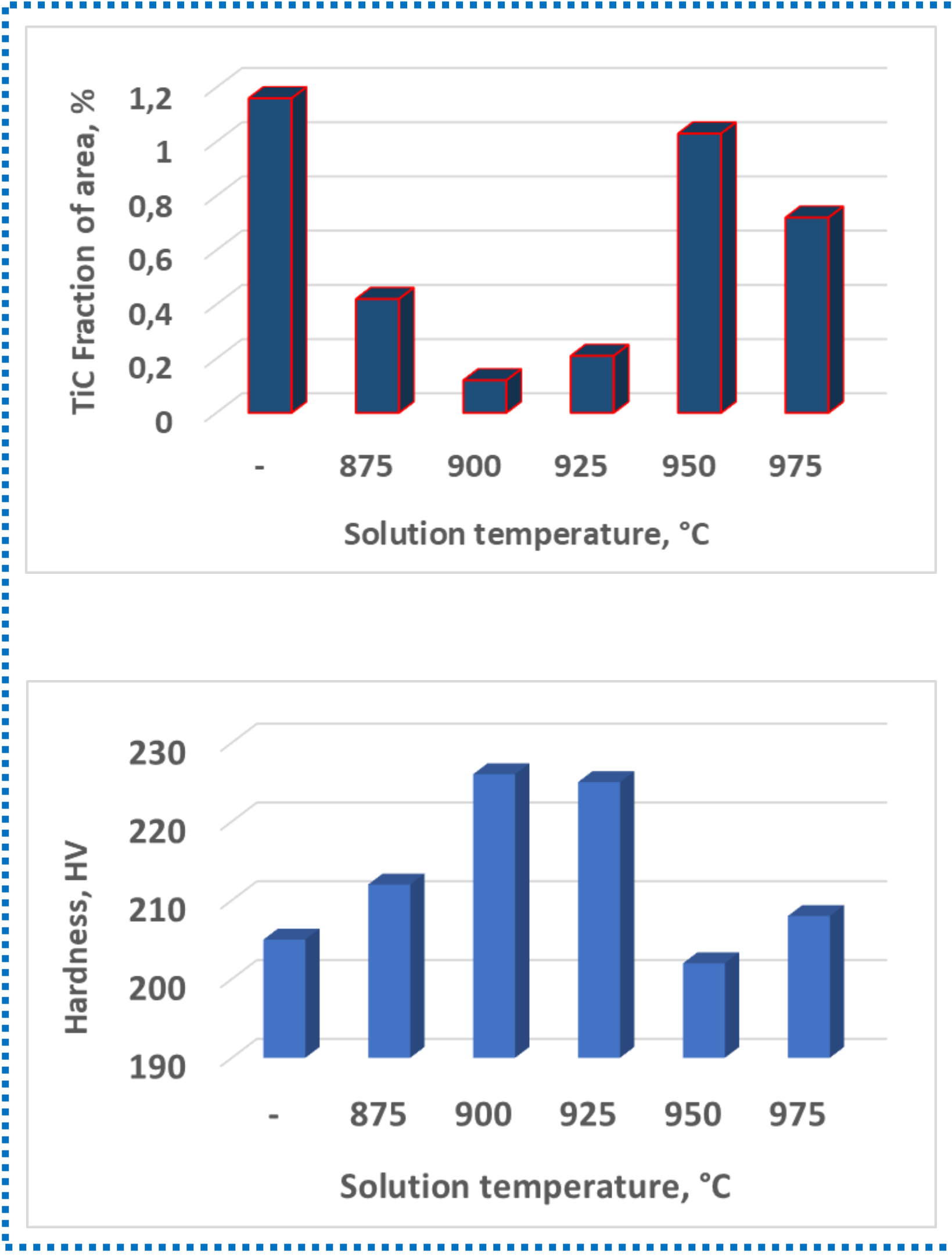
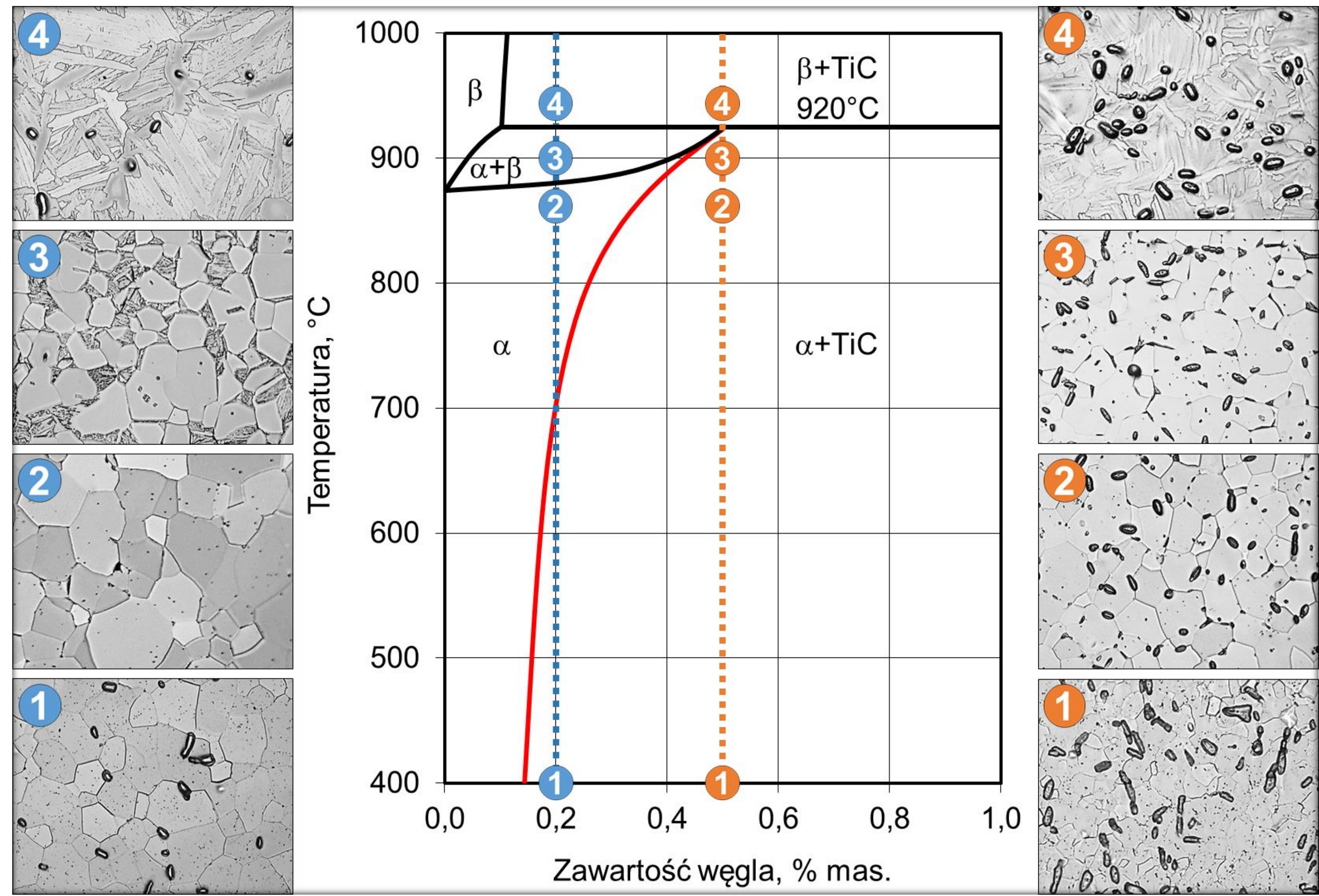
0.5%C ➡ $L \rightarrow L + \text{TiC} \rightarrow \beta + \text{TiC} \rightarrow \alpha \rightarrow \alpha + \text{TiC}$



After hot working

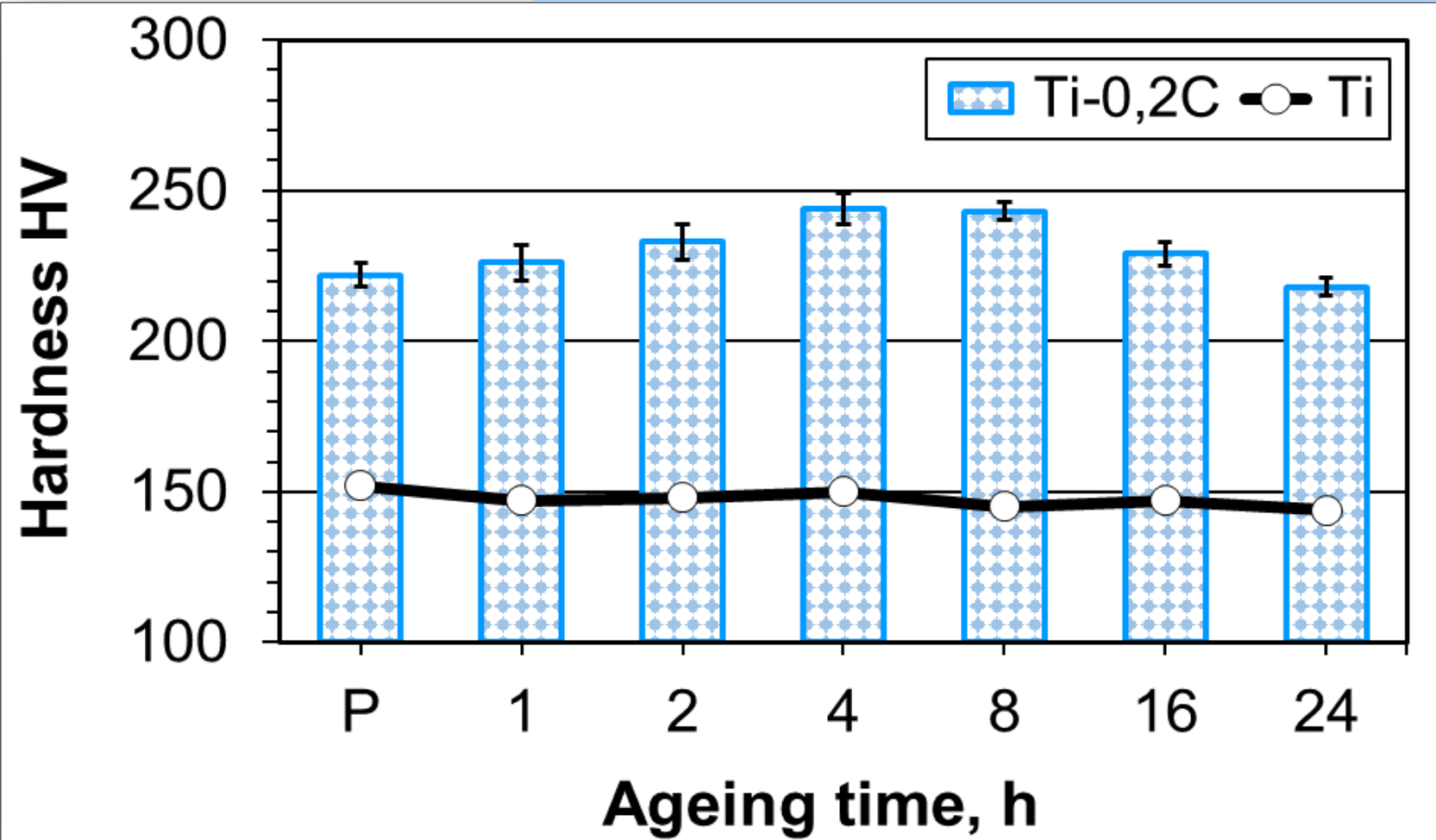
After annealing

Whether Ti can be solutioned by carbon?

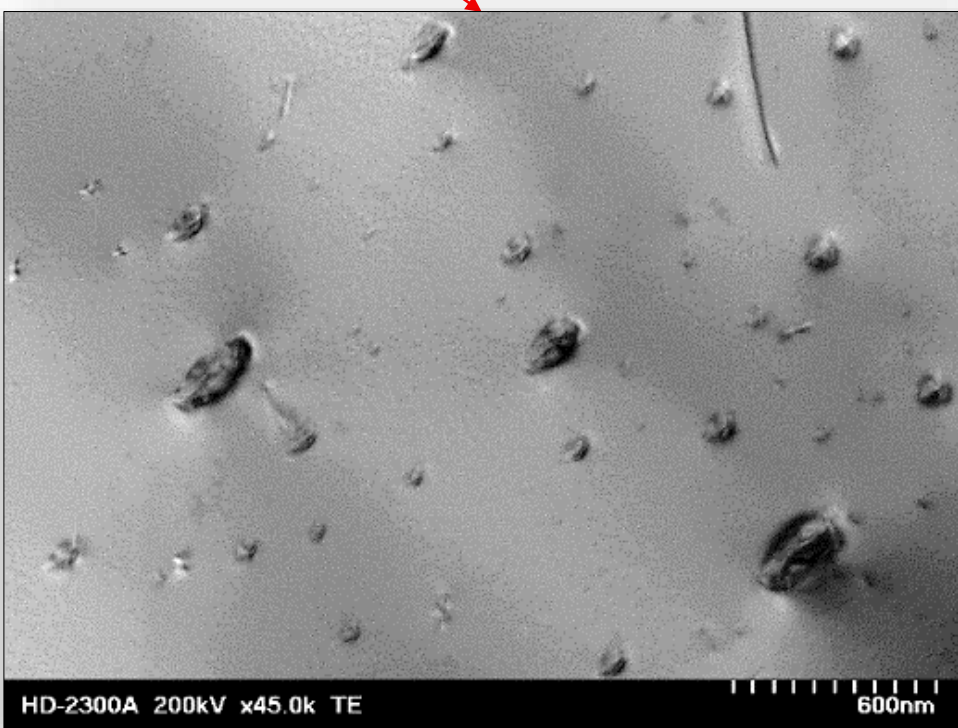
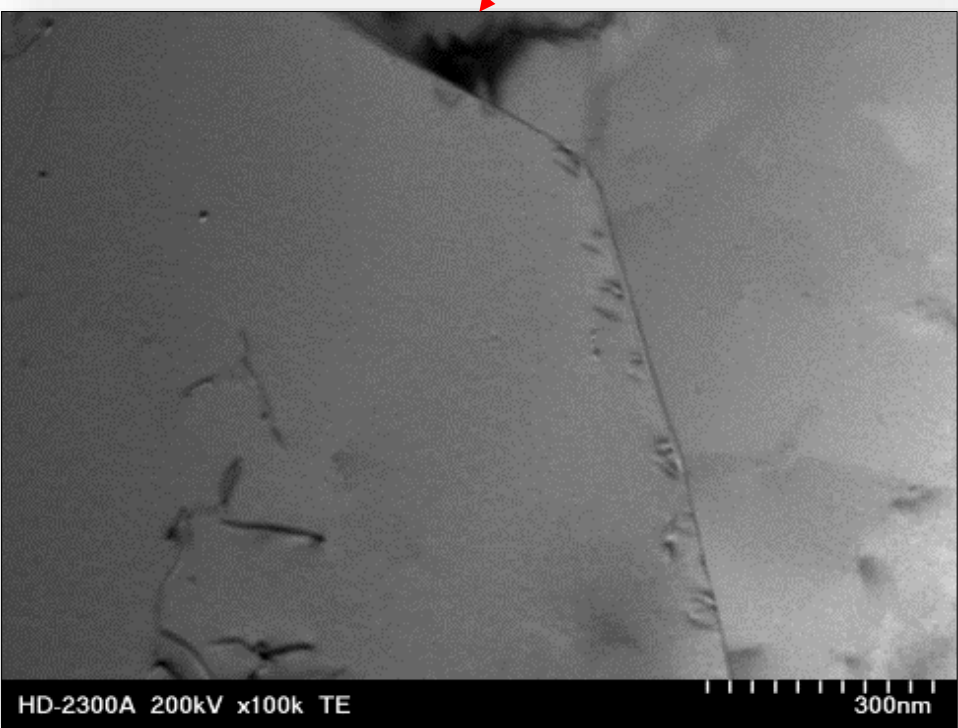
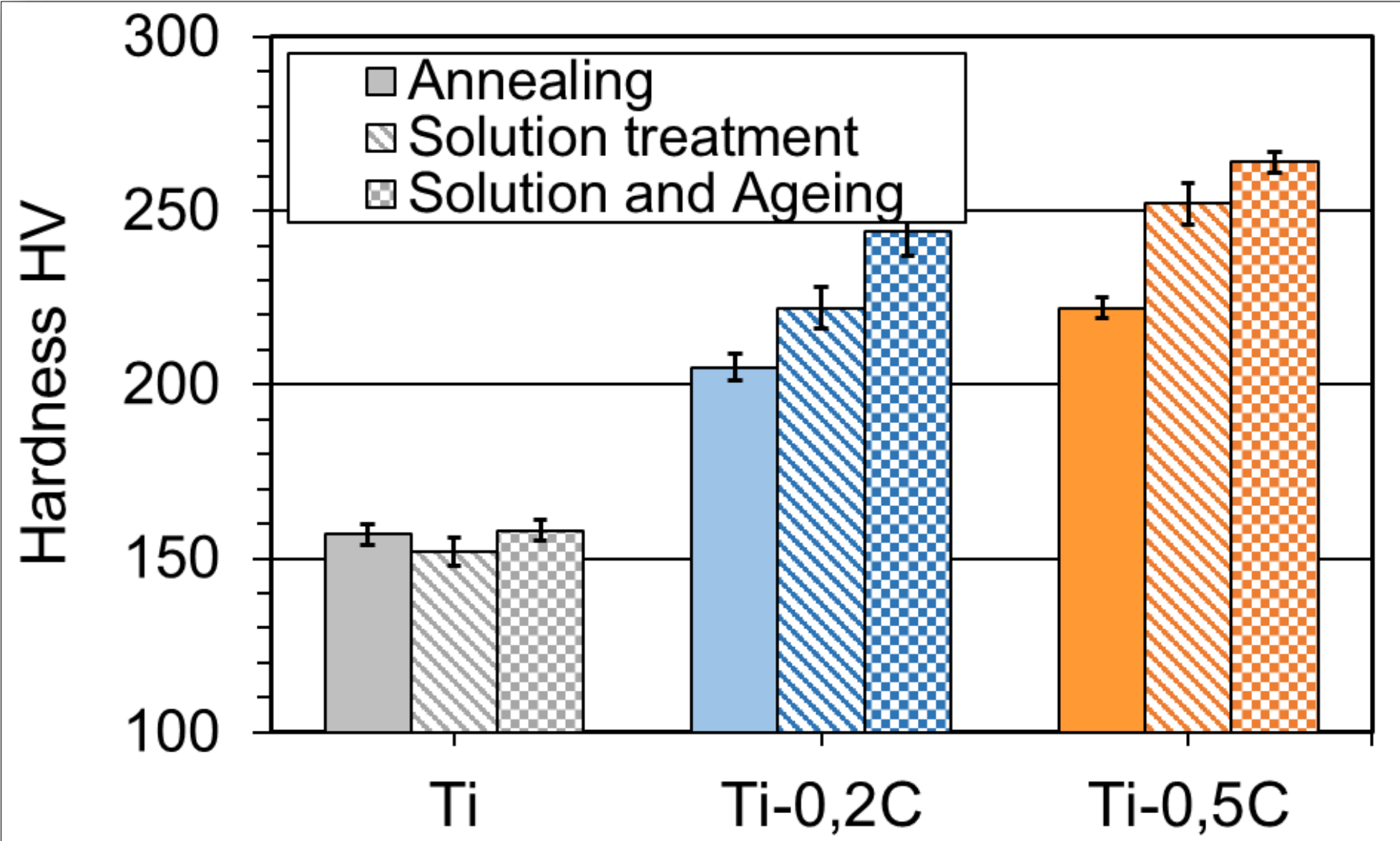
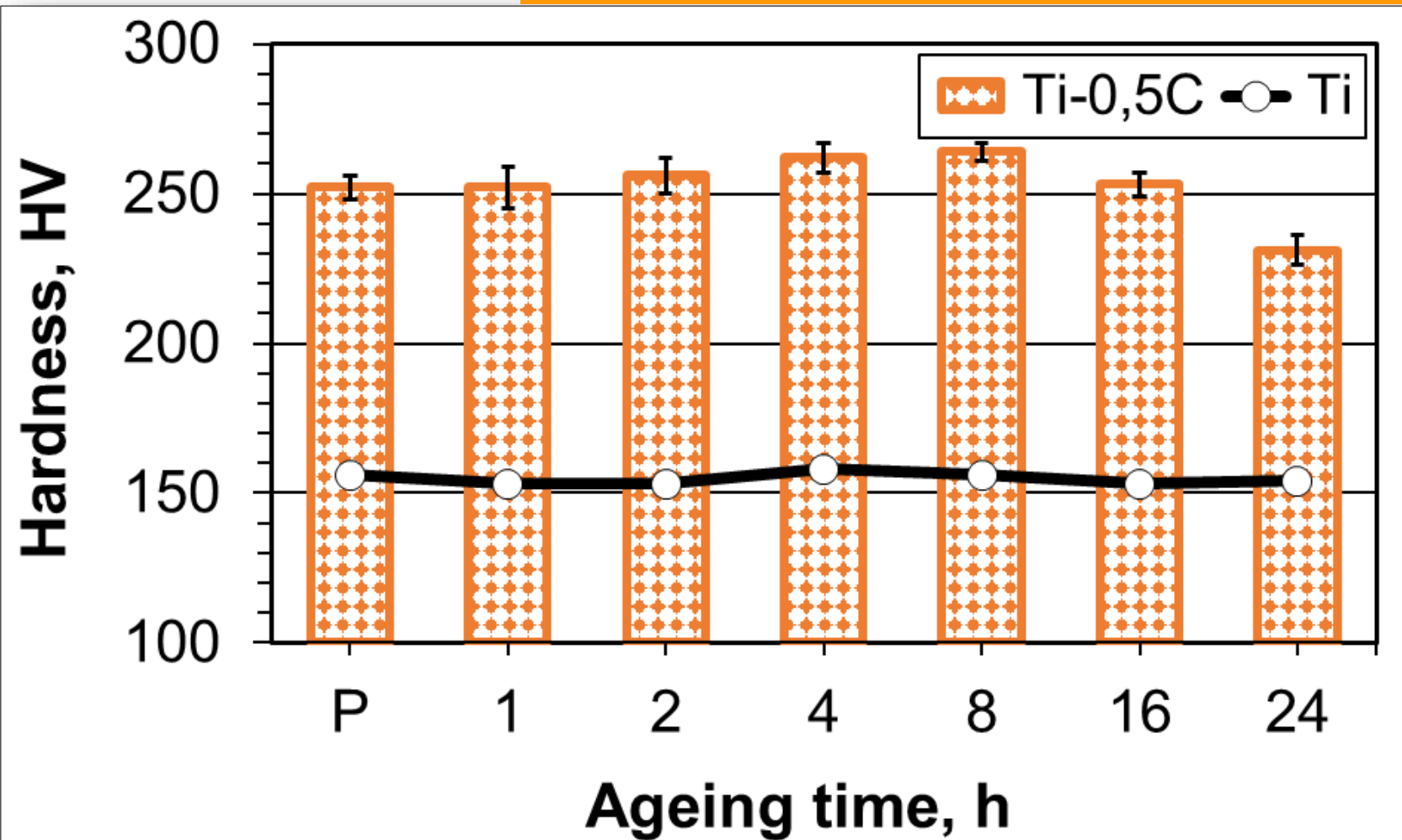


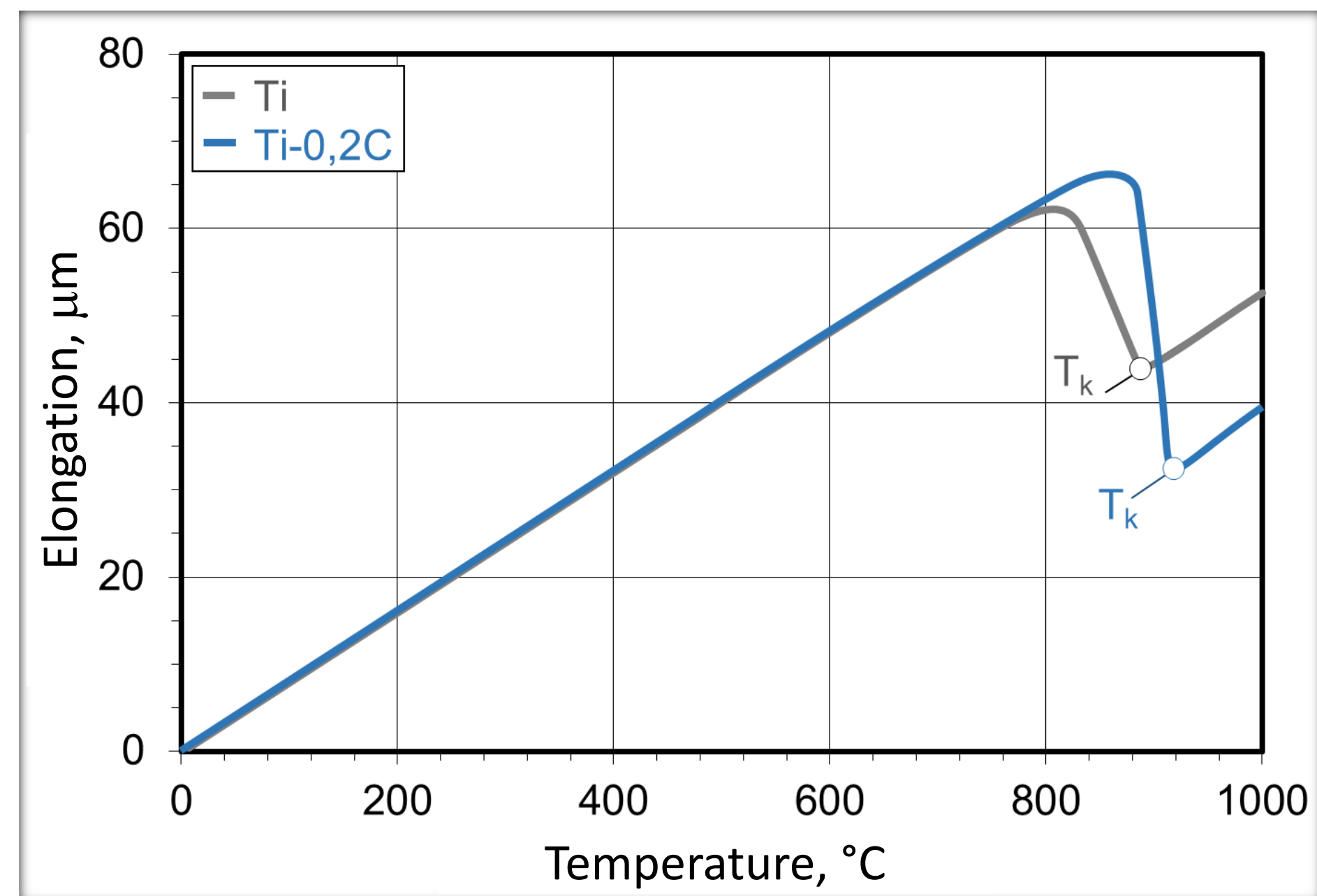
Age-hardening of Ti-0.2 (0.5)C

875°C/1h/water+550 °C/4h/air



900°C/1h/water+550°C/8h/air





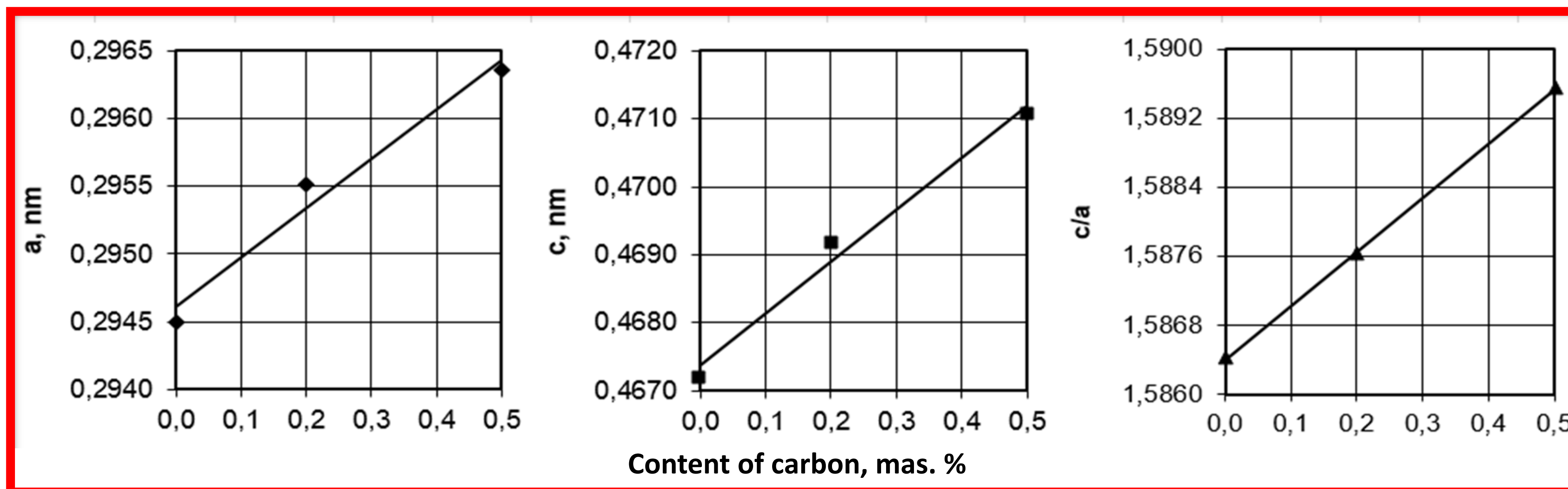
Alloy	Phase composition	Transformation temperature, °C	Carbon content. mas.%		
			0.0	0.2	0.5
Ti	α	$\alpha \rightarrow \beta$	890	920	945
Ti-5Al-2.5Sn			1035	1060	-
Ti-8Al-1Mo-1V	$\alpha + (\beta)$	$\alpha + \beta \rightarrow \beta$	1040	1060	-
Ti-6Al-4V	$\alpha + \beta$		975	995	1010
Ti-15Mo-3Nb-3Al-0.2Si	$\beta + (\alpha)$		810	825	-
Ti-33Mo	β		not apply		

Effect of carbon on the lattice parameters

Alloy	Lattice parameters. nm				
	a_α	c_α	c_α/a_α	a_β	a_{TiC_x}
Ti	0.2945	0.4672	1.5864		
Ti-0.2C	0.2952	0.4686	1.5874		0.4308
Ti-0.5C	0.2964	0.4711	1.5895		0.4311

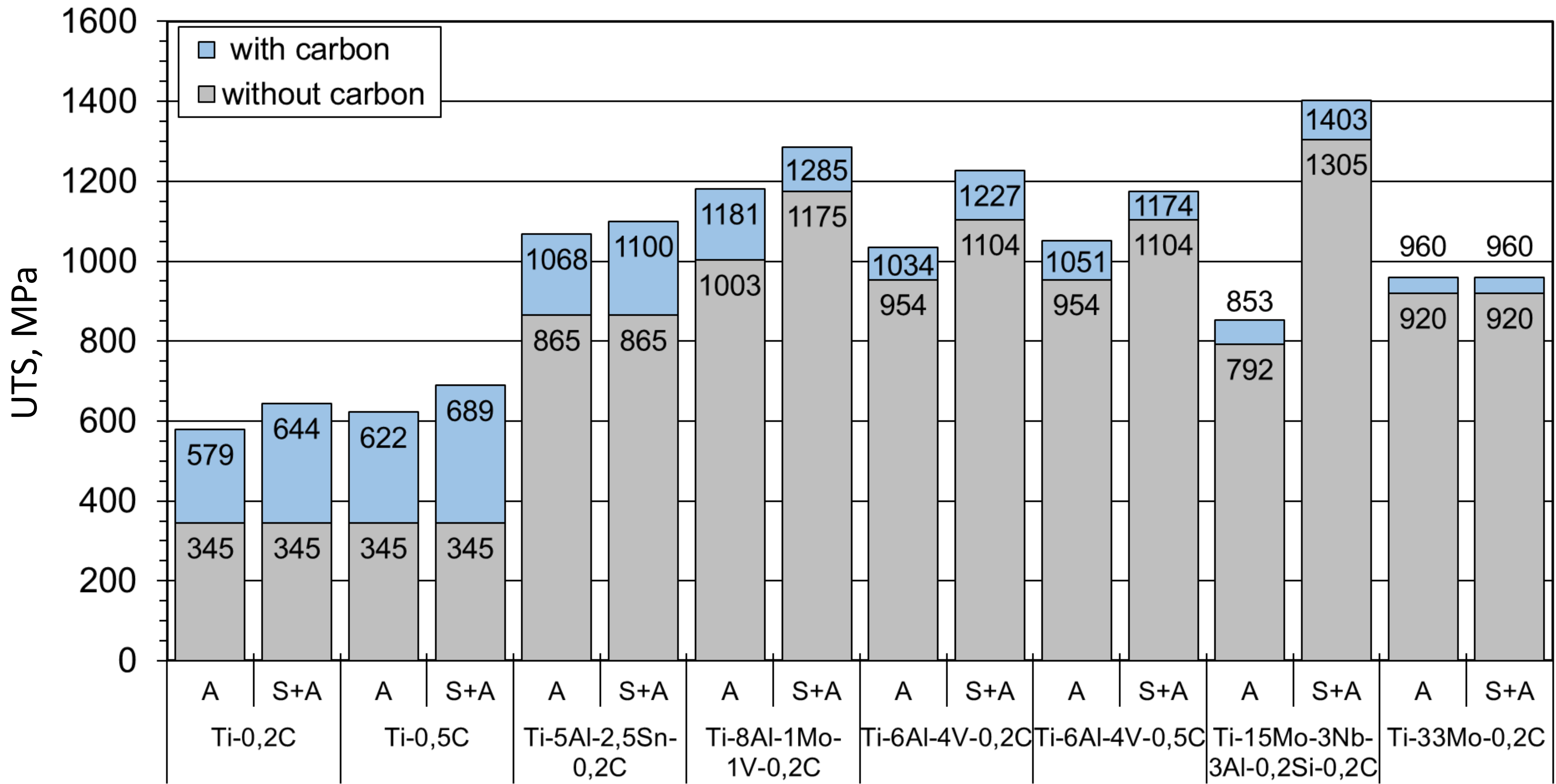
$$c_\alpha/a_\alpha = 1.595$$

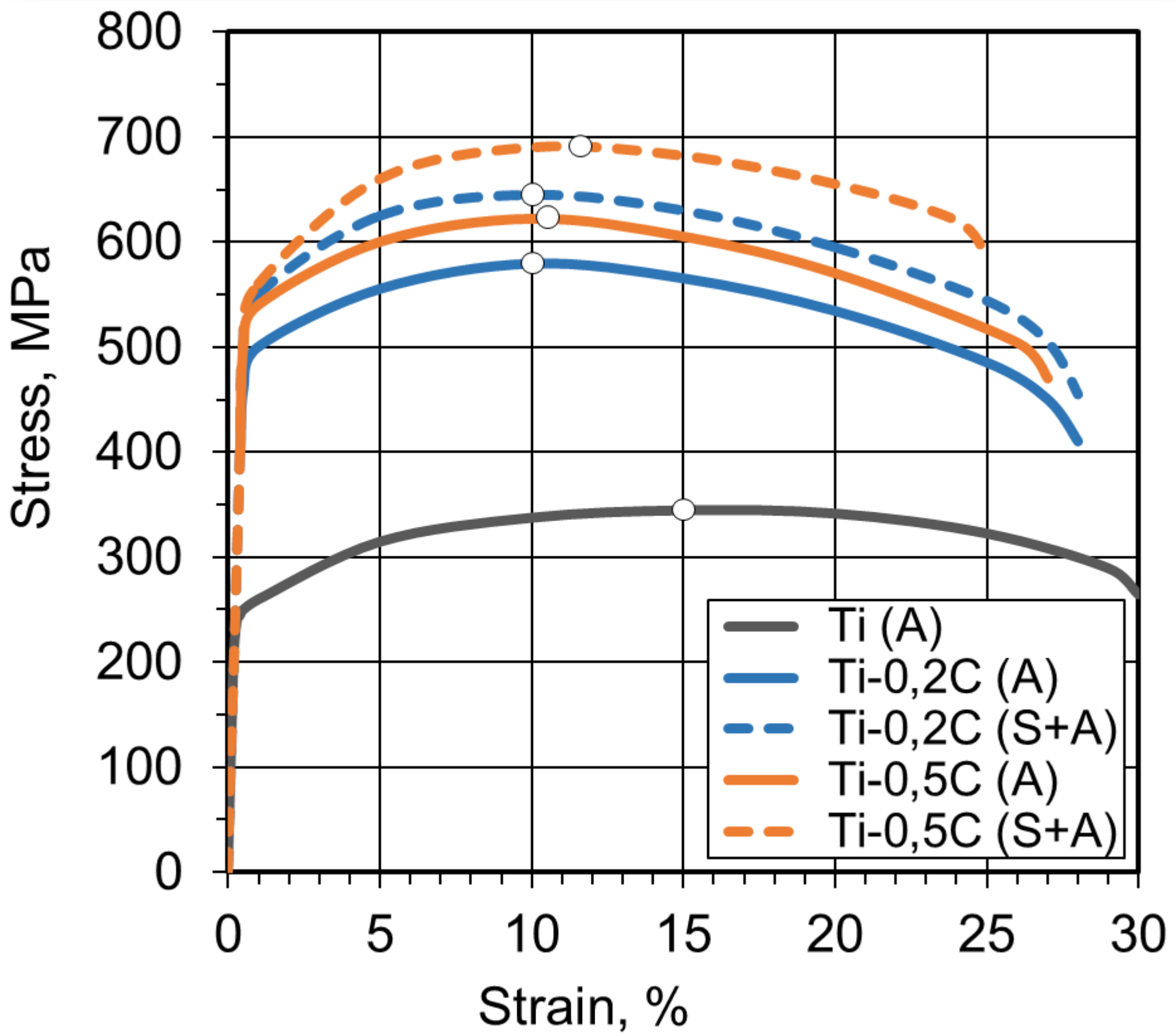
Limit of the good deformability of titanium alloys



Naka S., Kubin L.P., Perrier C.: The plasticity of titanium at low and medium temperatures. „Philosophical Magazine A”. Vol. 63. 1991. p. 1035.

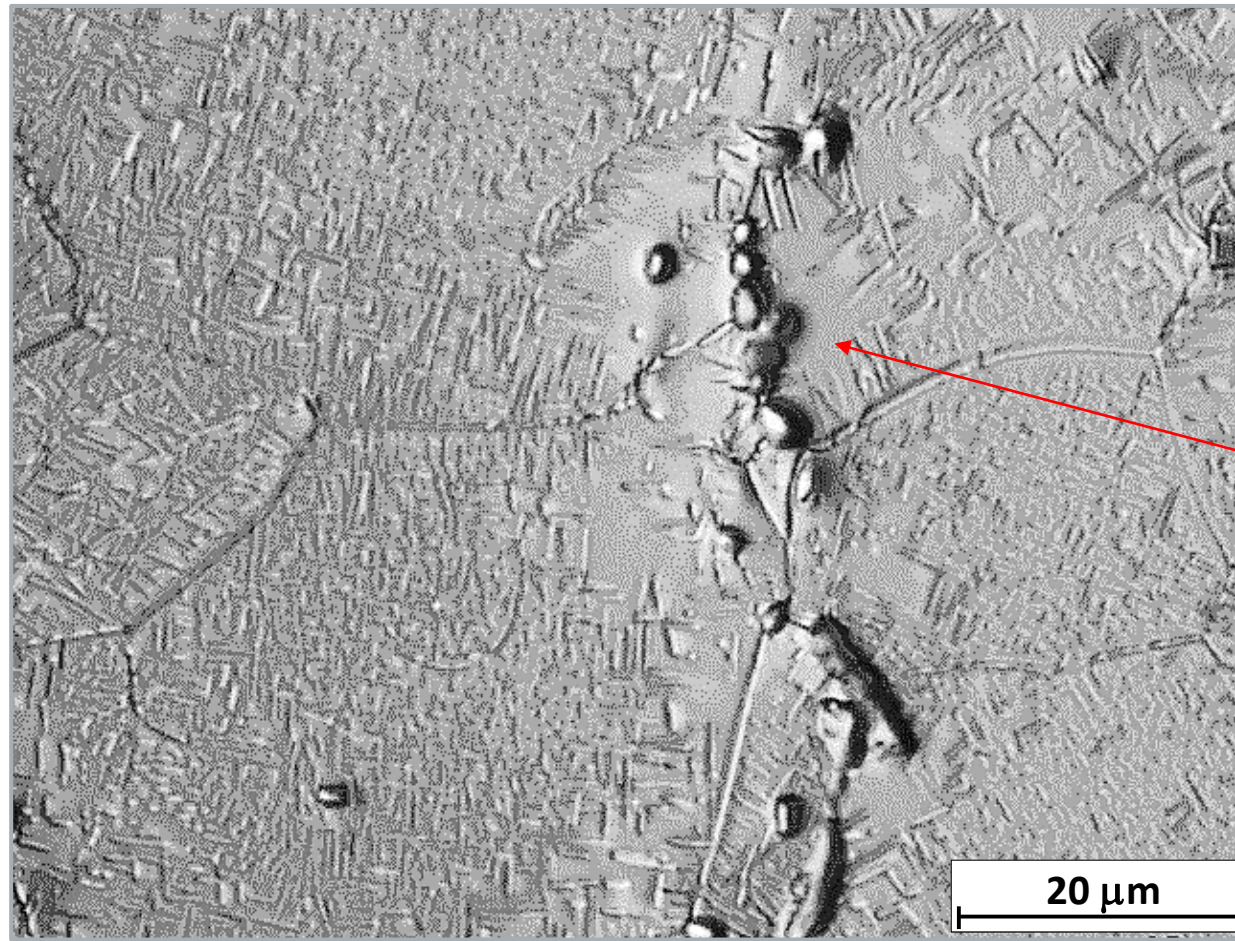
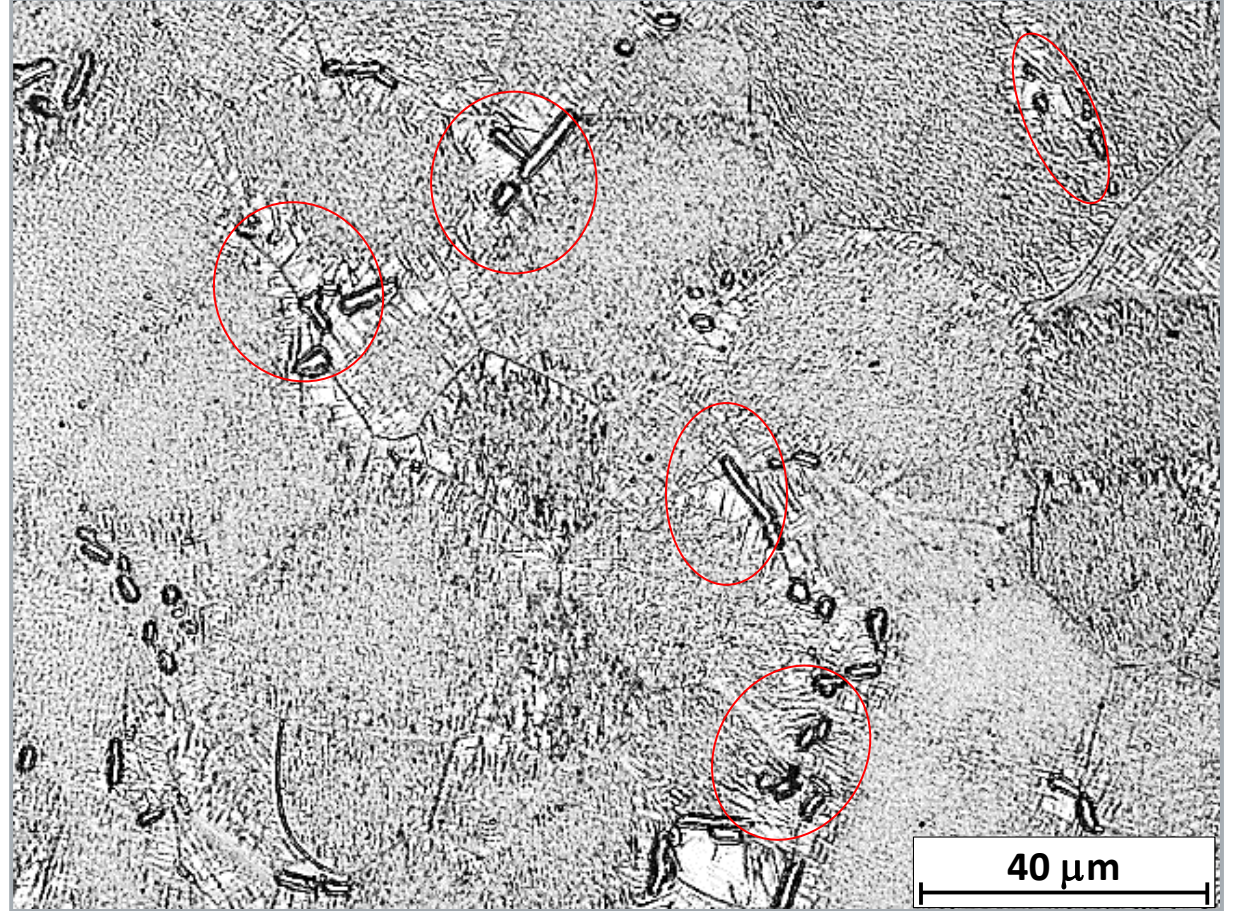
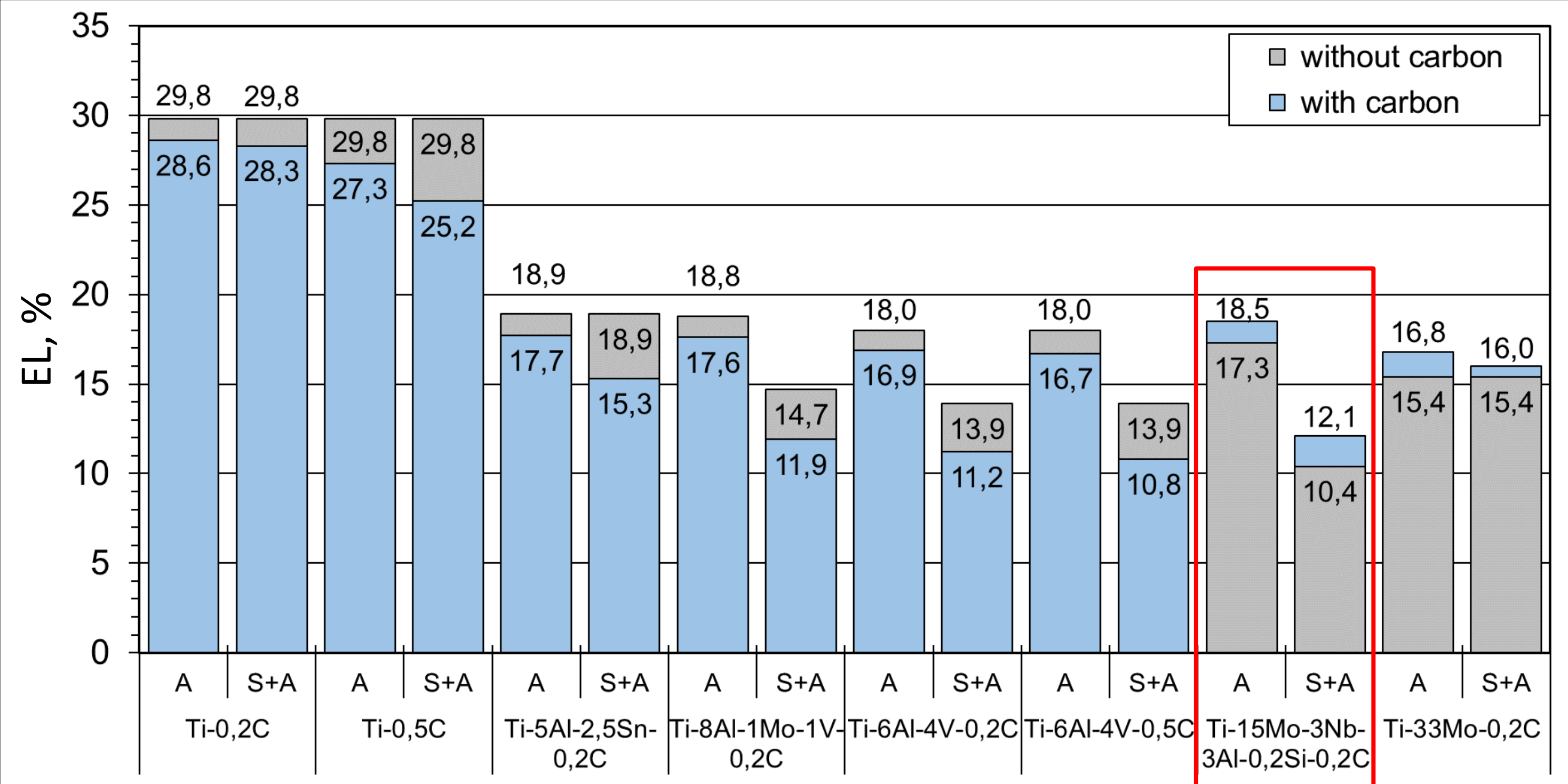






Alloy	State	UTS	YS	EL	RA
		MPa		%	
Ti	A	345	245	29.8	51.5
Ti-0.2C	A	579	496	28.6	48.6
	STA	643	554	28.3	46.6
Ti-0.5C	A	622	544	27.3	44.8
	STA	689	561	25.2	36.9
Ti Grade 1*	A	240	170	25.0	35.0
Ti Grade 4*	A	550	485	15.0	30.0

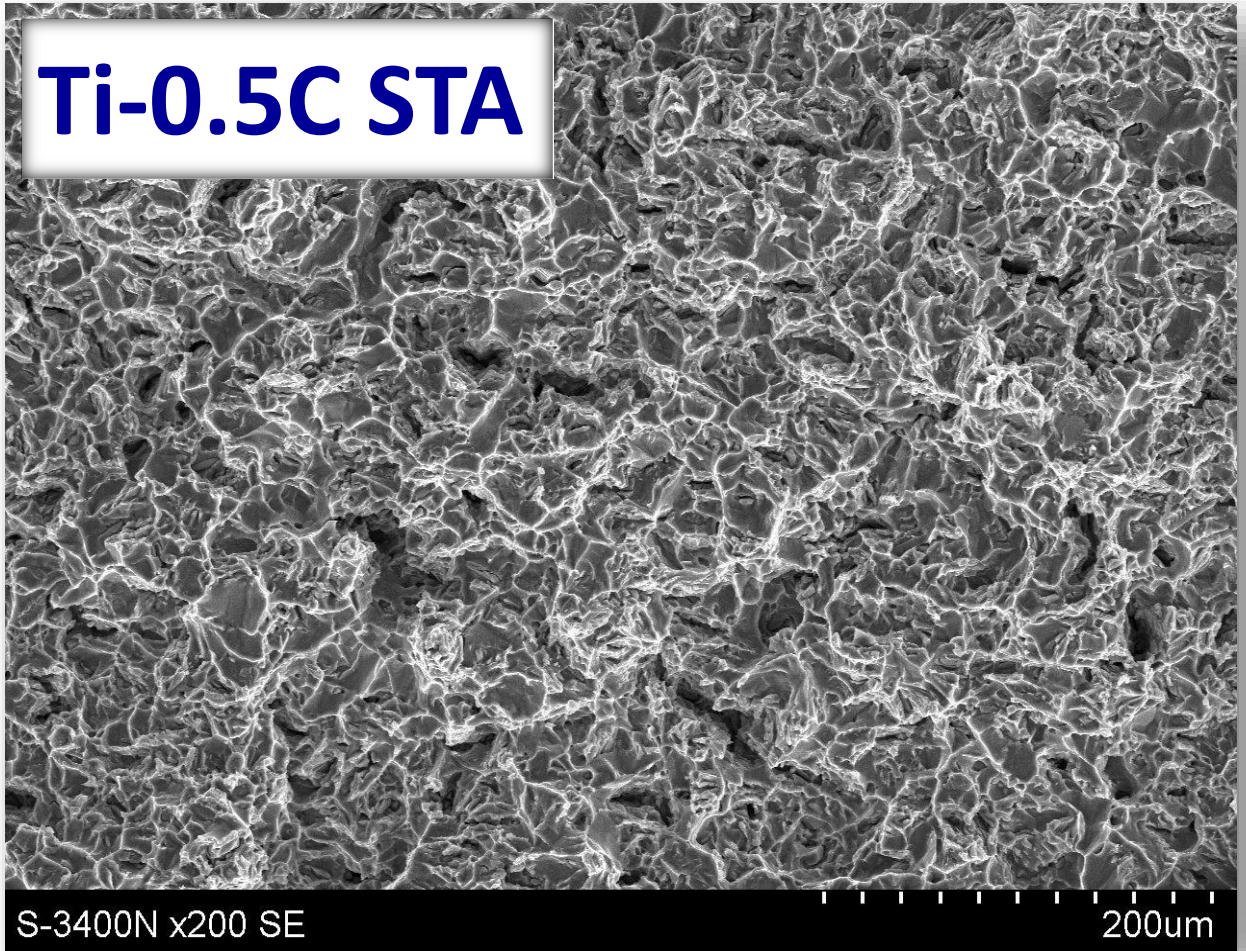
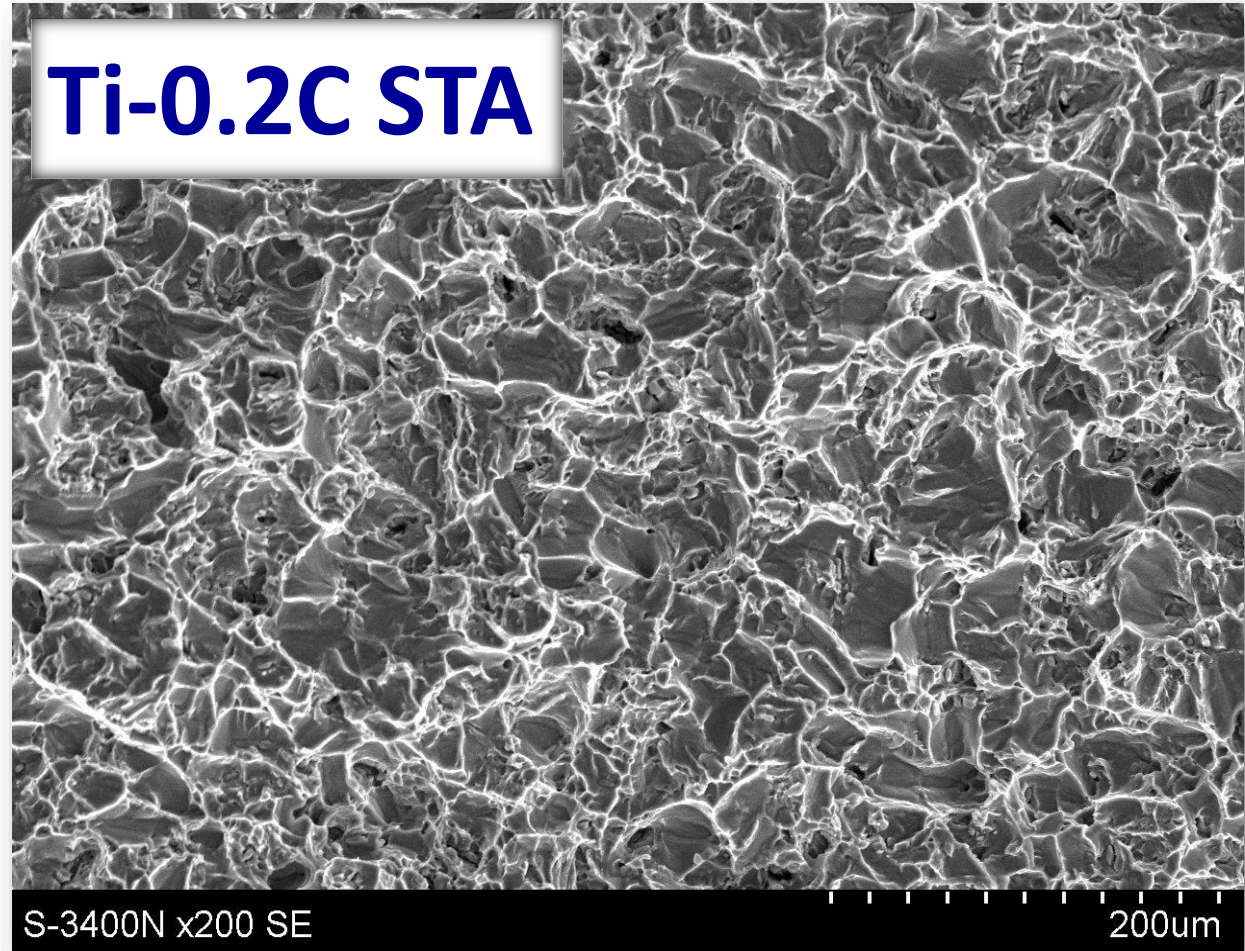
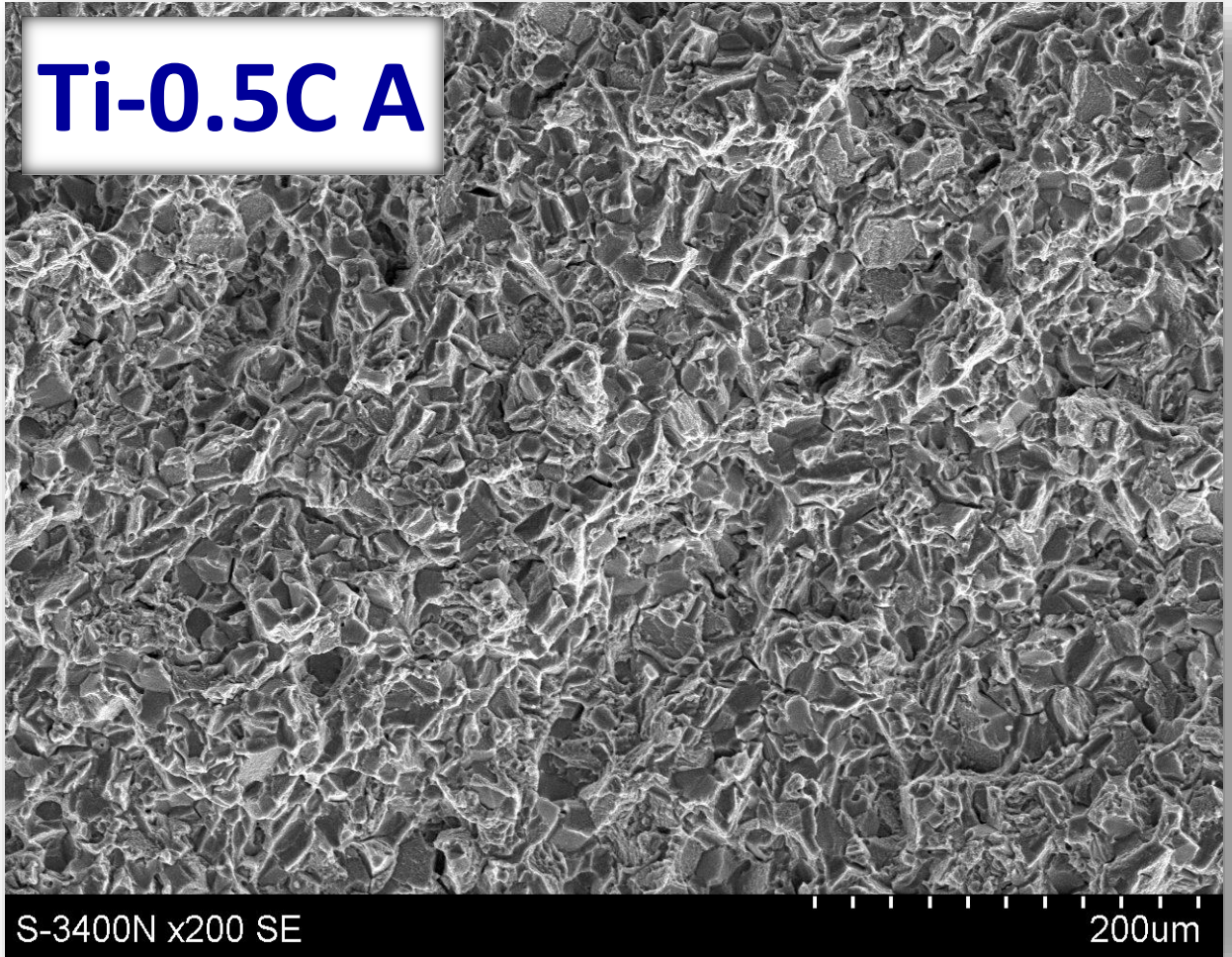
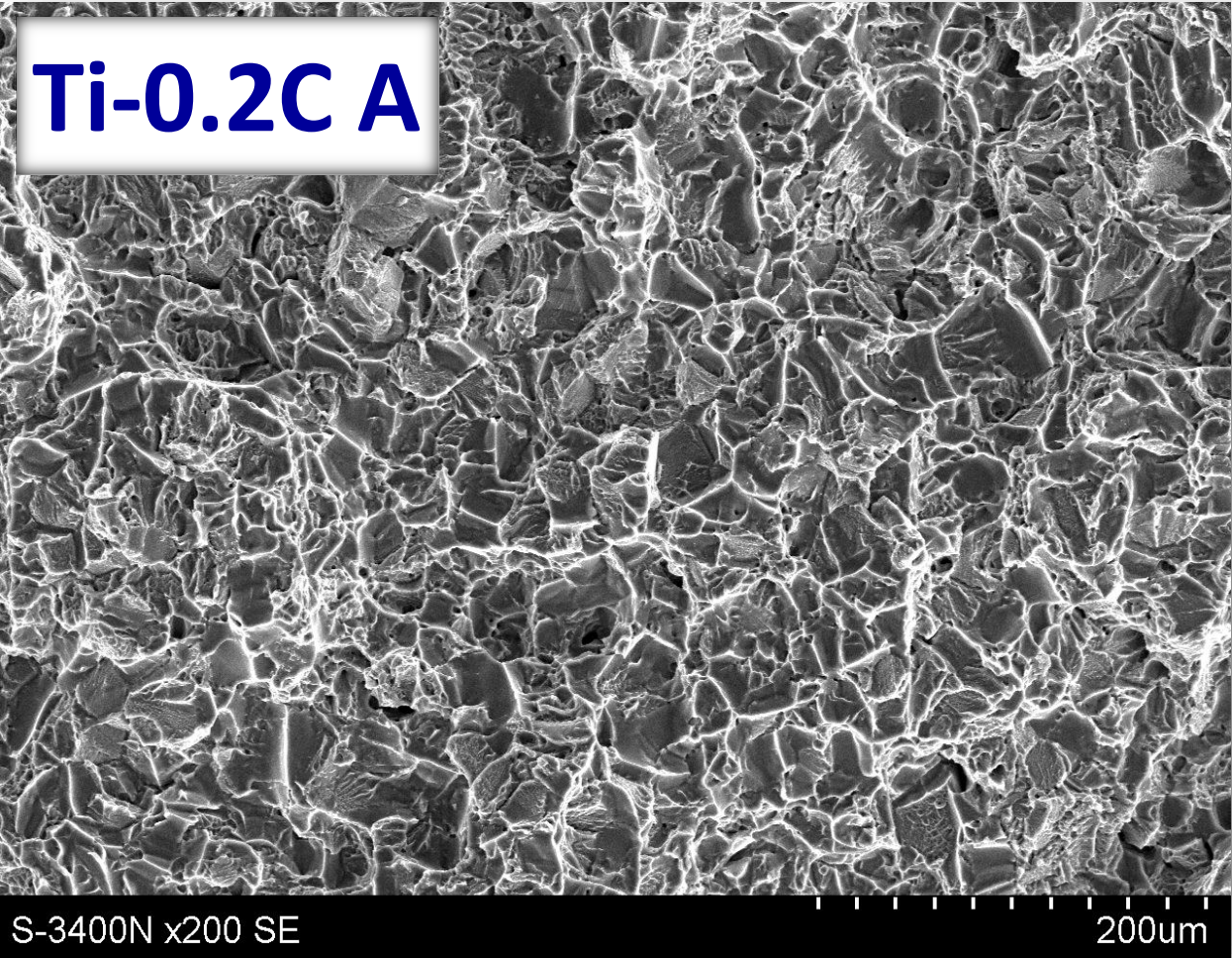


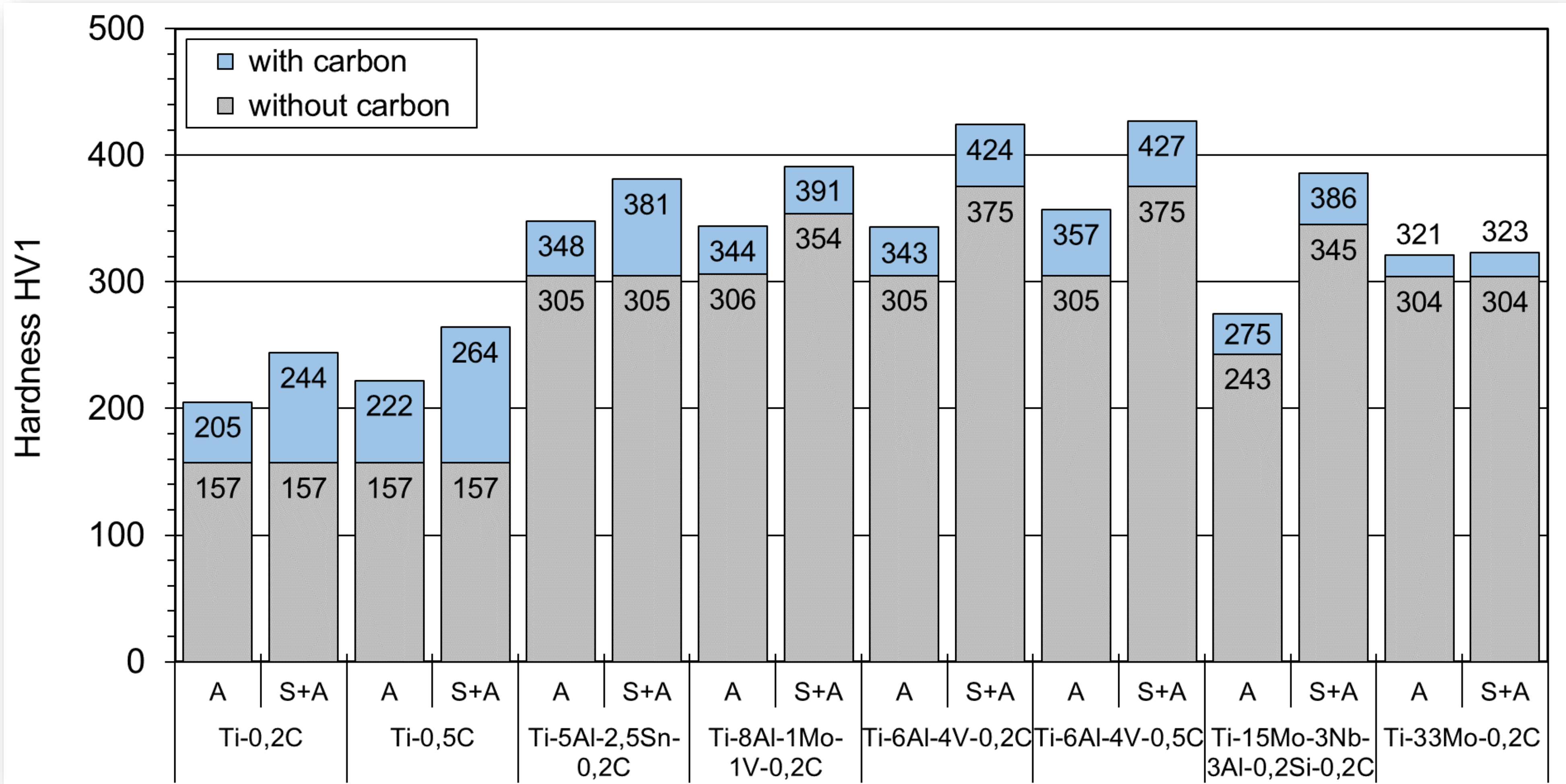


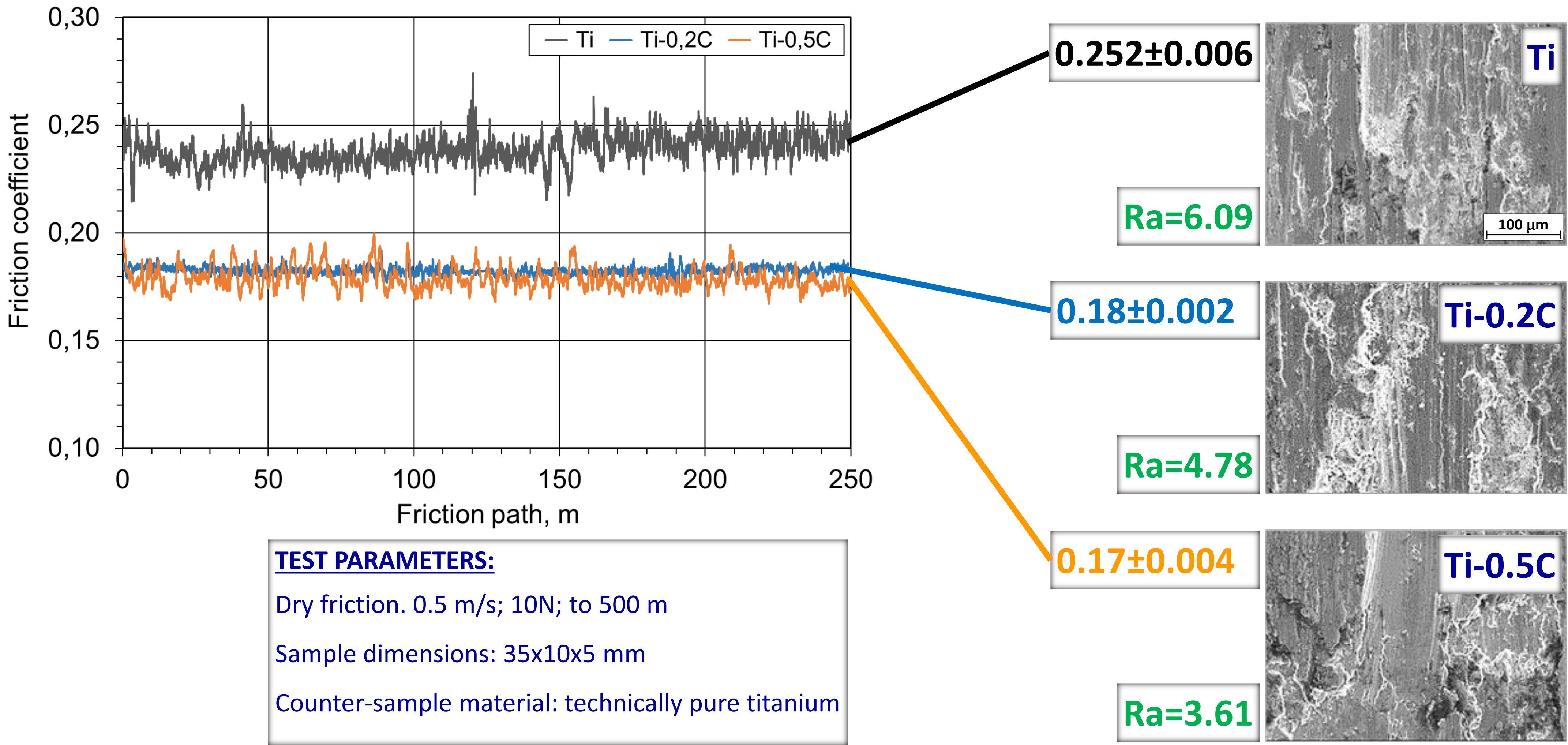
Carbide as „oxygen scavenger“

- traps oxygen atoms in place of the vacant lattice point in the carbon sublattice
- Decrease the oxygen content in the matrix

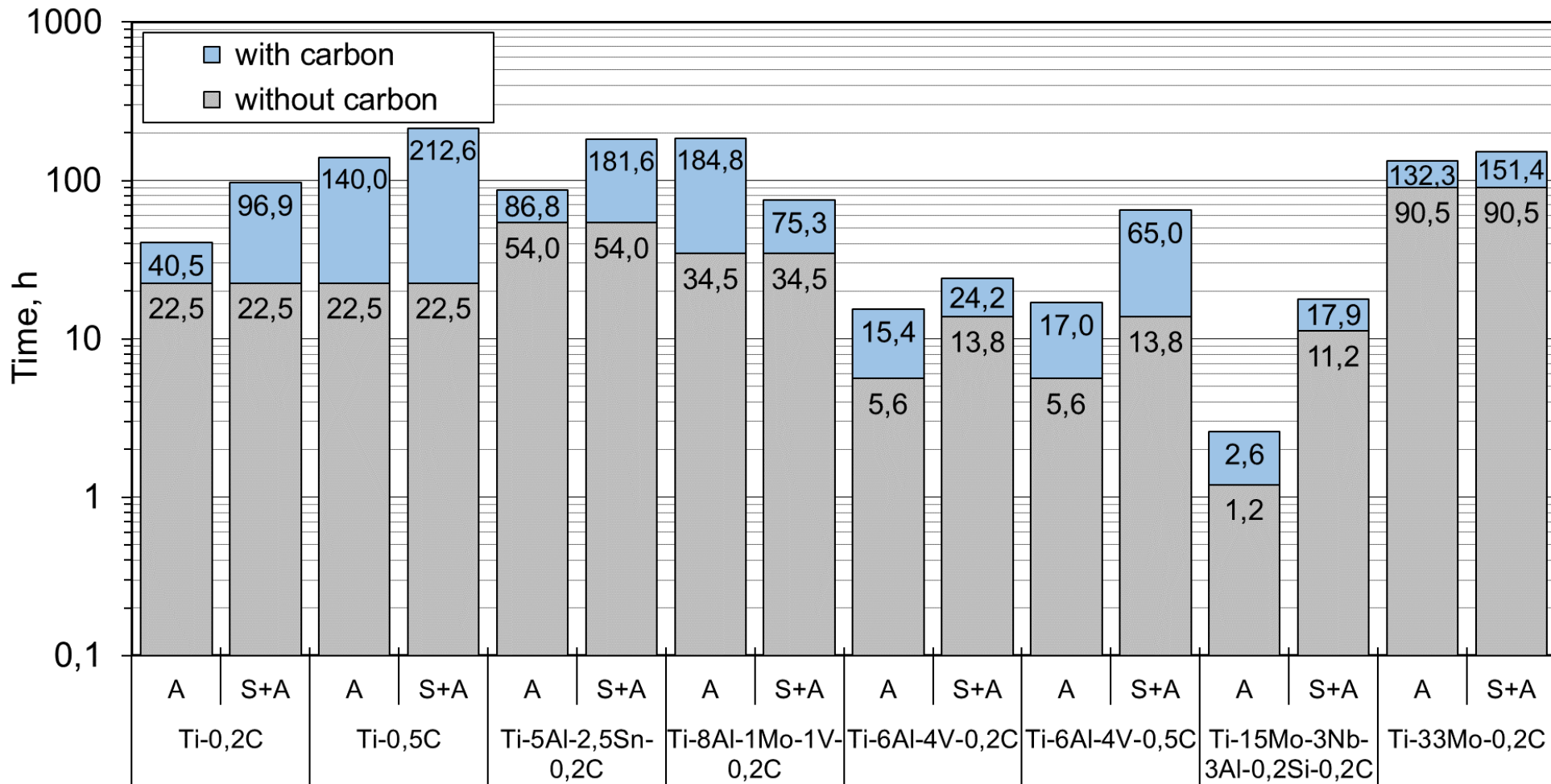
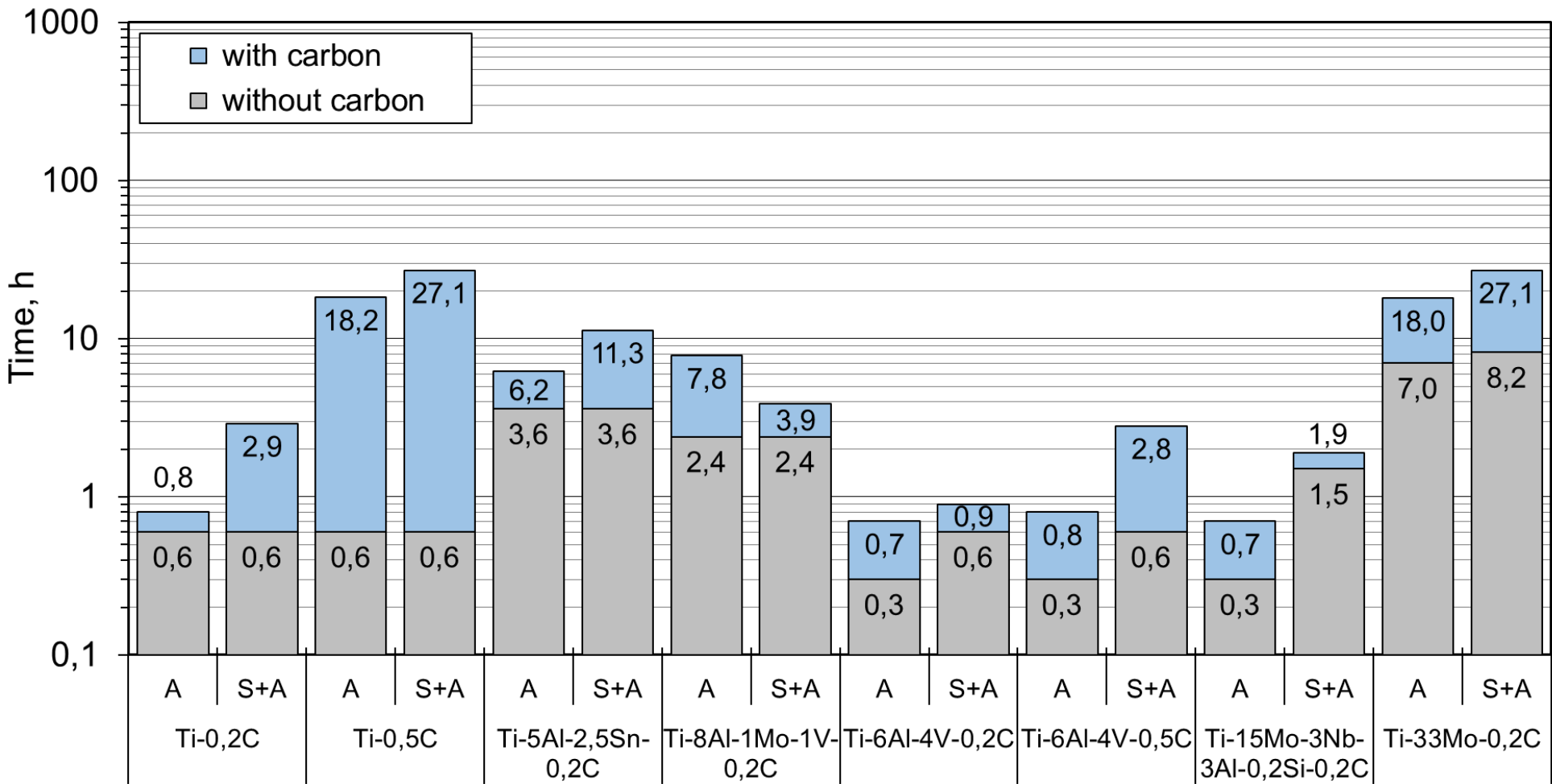
Alloy	State	KV. J
Ti	A	84.5
Ti-0.2C	A	67.0
	STA	54.5
Ti-0.5C	A	28.5
	STA	18.0
Ti Grade 1*	A	50.0
Ti Grade 4*	A	20.0



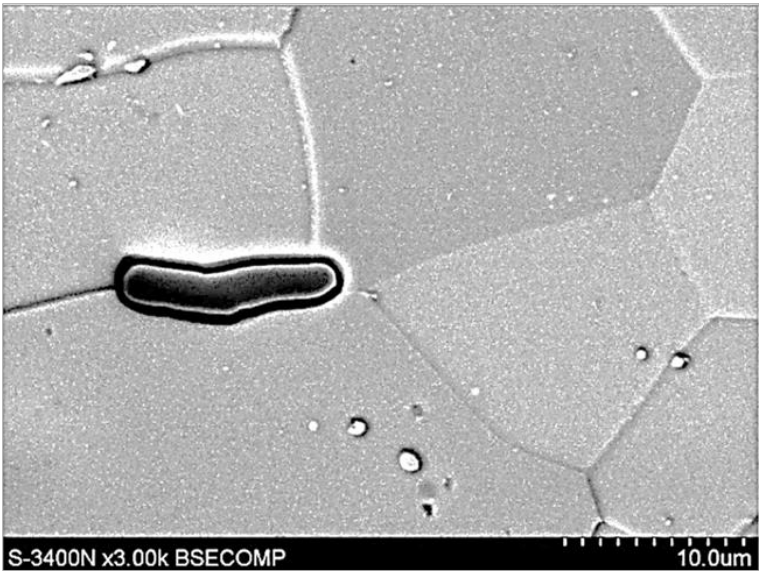




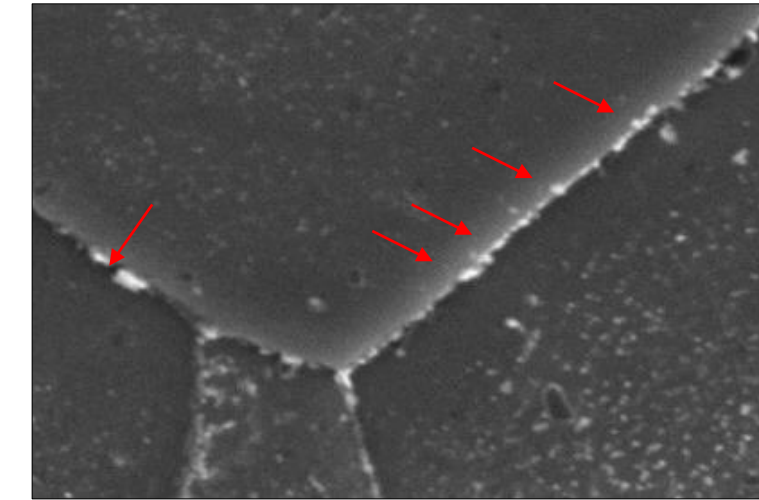
Effect of carbon on the creep resistance of titanium alloys



Primary carbides

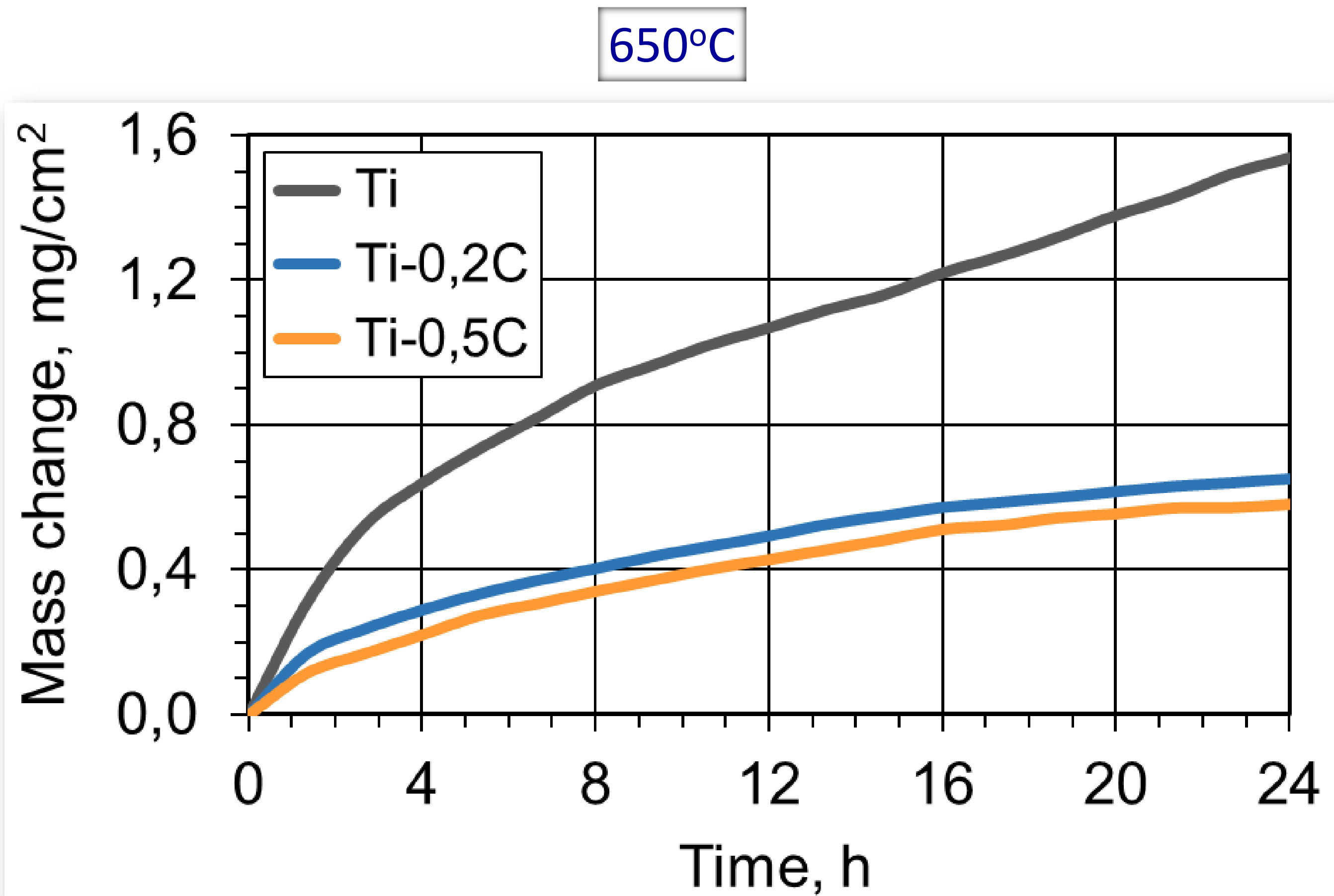


Secondary carbides



Alloy	State	Temperature °C	Strain MPa	Creep time to stress. h						Steady state creep rate, s ⁻¹
				0.1%	0.2%	0.5%	1.0%	2.0%	5.0%	
Ti (Grade 1)	A	400	170	0.1	0.6	8.4	22.5	45.8	73.4	0.000355
Ti-0.2C	A	400	170	0.1	0.8	13.2	40.5	85.0	193.0	0.000171
	STA			0.1	2.9	48.3	96.9	175.4	-	0.000067
Ti-0.5C	A	400	170	4.1	18.2	69.5	140.0	-	-	0.000058
	STA			5.9	27.1	97.4	212.6	-	-	0.000043

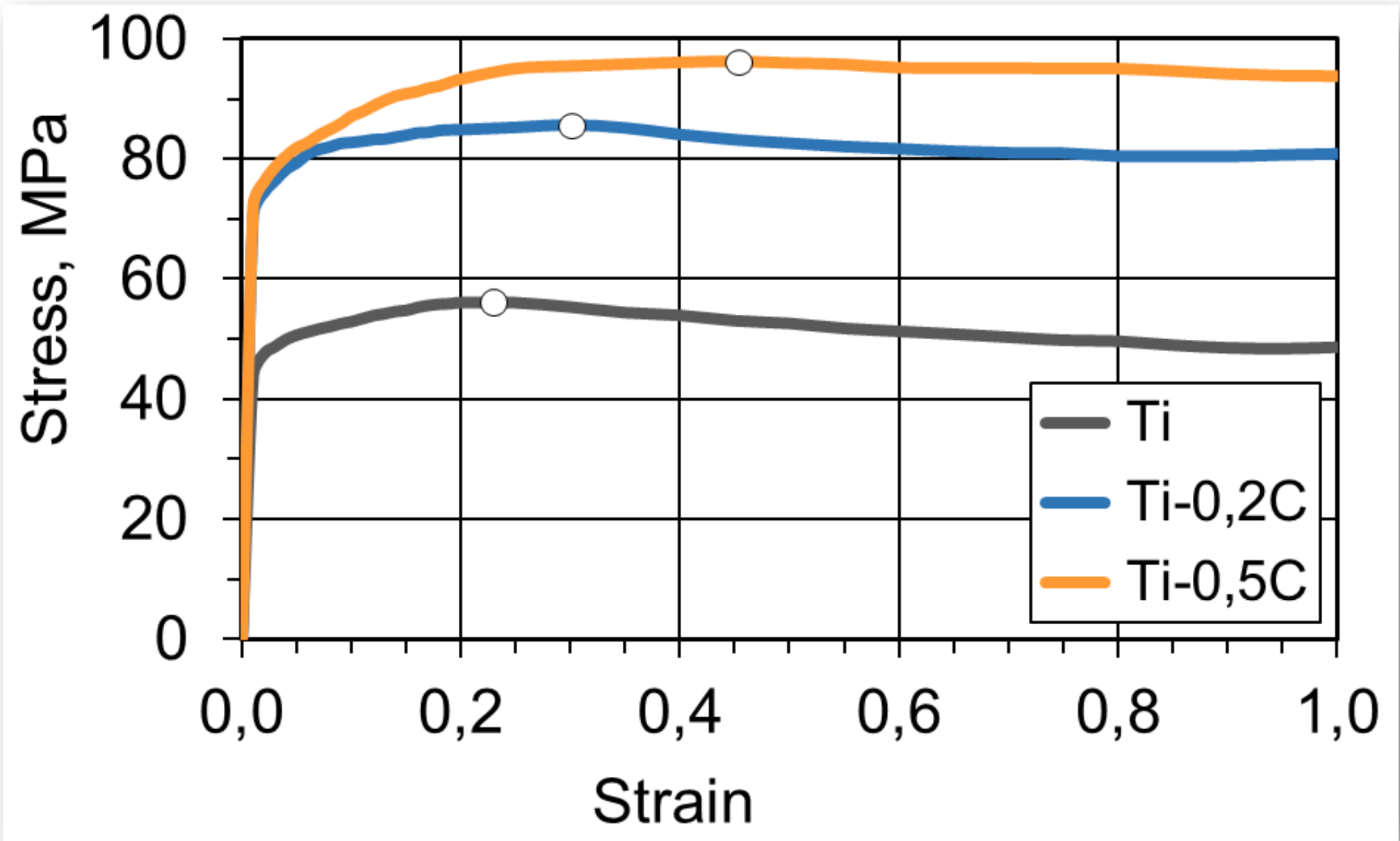




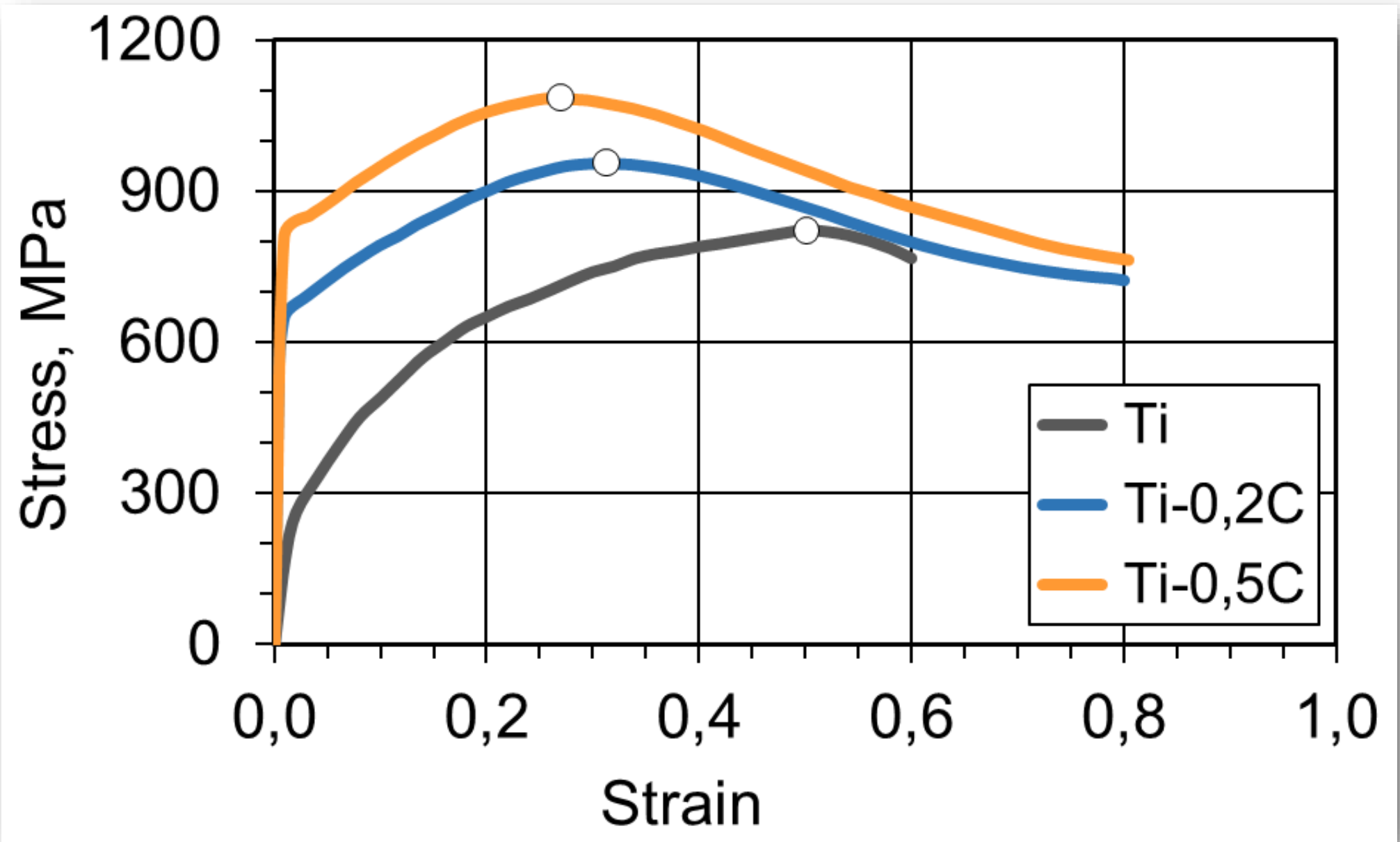
Reasons:

- decrease of oxygen diffusion activity by limiting its solubility in the interstitial spaces of the phases and occupied by carbon atoms
- decrease of oxygen content in the alloy matrix caused by the transfer of oxygen atoms from the matrix to the vacance in the carbon sublattice of non-stoichiometric TiC_x carbides.

T = 890°C



T = RT



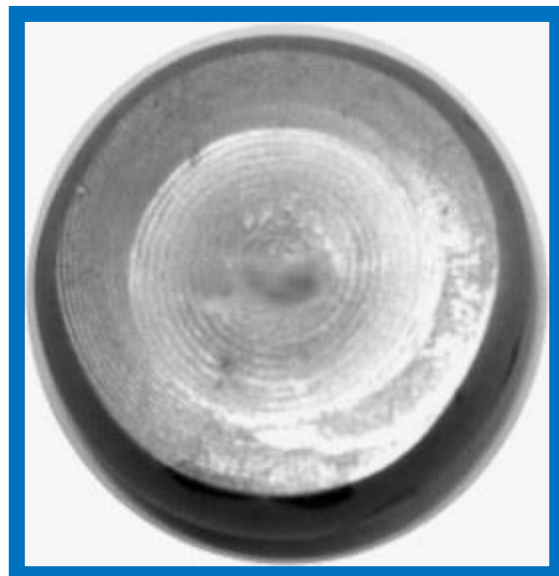
Ti-0.2C



Ti-0.5C

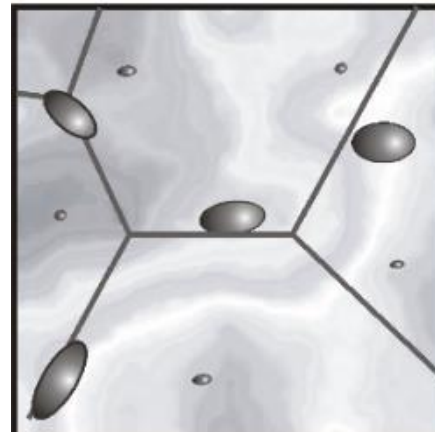
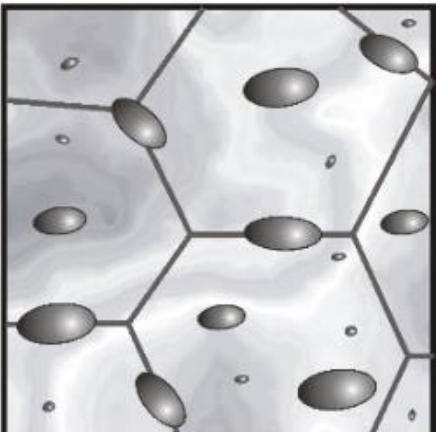


Ti-0.2C



Ti-0.5C



<0.08%C	0.2%C	0.5%C
		
Tensile strength	++	+/-
Elongation	+/-	-
Young's modulus	+	+
Hardness	++	+
Impact Energy	-	--
Creep resistance	+	++
Oxidation resistance	+	++
Corrosion resistance	+/-	-
Wear resistance	+	+
Hot formability	+/-	-
Cold formability	-	--
Hardenability by heat treatment	+	+
Microstructure stability	+	+
Susceptibility to grain growth	+	++

Effect of 0.2% C on the properties of titanium alloys

Parameter	Effect of 0.2 mas. % C in titanium alloys					
	Ti	α	near- α	$\alpha+\beta$	near- β	β
Tensile strength	+++	++	++	+	+	+
Yield strength	+++	++	++	+	+	+
Elongation	-/+	-/+	-/+	-/+	+	+
Young's modulus	+	+	+	+	+	+
Hardness	+++	++	++	+	+	+
Impact energy	-	--	--	--	--	-
Creep resistance	+++	+++	+++	+	+	++
Oxidation resistance	+++	+	+	++	+	+
Corrosion resistance	-/+	-/+	-/+	-/+	-/+	+/-
Hot formability	-/+	-	-	-	-	-
Cold formability	-/+	--	--	--	--	-
Wear resistance	+	+	+	+	+	+
Hardenability in heat treatment	++	++	+	+	+/-	+/-
Microstructure stability	+	+	+	+	+	+
Susceptibility to grain growth	+	+	+	+	++	++
Transformation temperature	+	+	+	+	+	



It depends from:

- **group of titanium alloys**
- **level of carbon content**
- **content of alloying elements (phase composition of alloy)**

within the controlled content of up to approx. 0.2 wt.%. carbon in titanium alloys is not an impurity, but a component that may have many useful functions which are different for different groups of alloys

The results achieved to date perhaps bring closer the time when some small addition of carbon to any titanium alloy will become a mandatory standard???



Research Team

Prof. dr hab. inż. Wojciech Szkliniarz,
Prof. dr hab. inż. Maria Sozańska,
Prof. dr hab. inż. Eugeniusz Hadasik,
Prof. dr hab. inż. Lucjan Swadźba
Prof. dr hab. inż. Janusz Szala
Dr hab. inż. Agnieszka Szkliniarz, prof. PŚ,
Dr hab. inż. Tomasz Rzychoń, prof. PŚ,
Dr hab. inż. Grzegorz Moskal, prof. PŚ,
Dr inż. Roman Przeliorz
Dr inż. Bartosz Chmiela,
Dr hab. inż. Kinga Rodak, prof. PŚ,
Dr inż. Tomasz Mikuszewski
Dr inż. Tomasz Pawlik
Dr inż. Rafał Michalik
Dr inż. Jacek Chrapoński
Dr inż. Barbara Juszczyk
Dr inż. Georg Jarczyk, ALD Vacuum Technologies, Hanau
Prof. Ivo Schindler, VSB Ostrava
Prof. Rudolf Kawalla, TU Bergakademie Freiberg

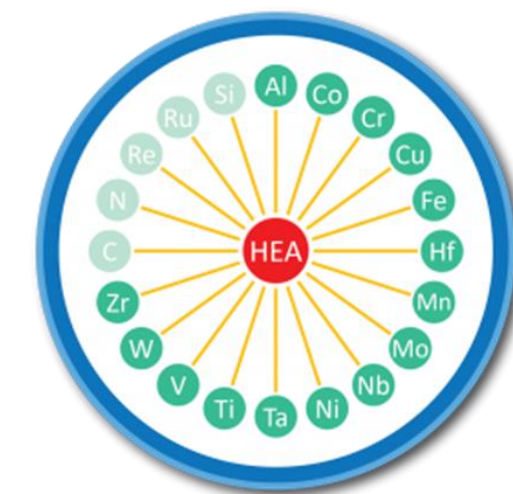
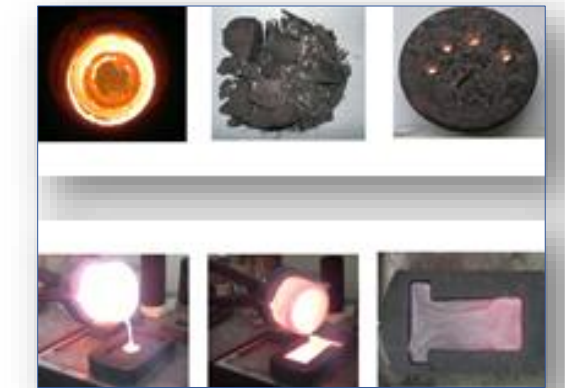
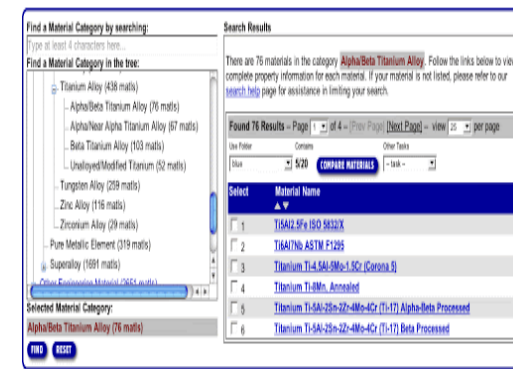
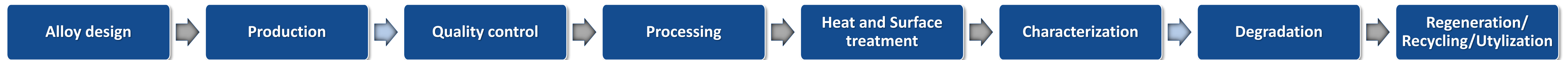


Technology Hall
ME Faculty of SUT



UCZELNIANA STREFA INNOWACJI MATERIAŁOWYCH

University Zone of Material Innovations (USTINMAT)



Areas of research: TiAl based alloys,
Low-cost titanium alloys,
Lightweight high entropy alloys,
New titanium alloys for medicine,
Hydrogen storage materials.

Thank You for attention



Silesian University
of Technology

